

RESIDENTIAL DEVELOPMENT

4-8 MARSHALL AVENUE, 1-5 CANBERRA AVENUE, & 2-8 HOLDSWORTH AVENUE, ST LEONARDS NSW

Prepared for:

EVERGREEN INVESTMENT HOLDINGS

Reference: P2160_02

16 February 2022

1 PROJECT BACKGROUND

Morrow Geotechnics Pty Ltd has undertaken a Geotechnical Investigation to provide geotechnical advice and recommendations for proposed development at 4-8 Marshall Avenue, 1-5 Canberra Avenue & 2-8 Holdsworth Avenue NSW (the site).

A previous investigation for the site a Due Diligence for Purchase phase was carried out by Morrow Geotechnics, reference P2160_01 dated 9 March 2021. The previous geotechnical investigation provided preliminary information from five boreholes drilled around the site perimeter.

1.1 Proposed Development

Architectural Drawings for the proposed development have not been provided at the time of preparation of this report. From discussions with the client, Morrow Geotechnics understands that the proposed development will likely comprise the construction of three residential structures over four levels of basement parking. Excavation for the basement is expected to extend up to a depth of approximately 12.5 m below existing ground level (mBGL).

1.2 Investigation Intent

The purpose of this investigation is to provide further geotechnical advice and recommendations specific to the ground conditions observed at site for the proposed development. In particular, the centre of the site has been investigated through difficult access drilling rigs.

The recommendations of this report include:

- Foundation advice along with relevant geotechnical design parameters;
- Excavation and shoring advice along with relevant geotechnical design parameters;
- Approaches to minimise the impact of the proposed development through vibration, ground movement or groundwater drawdown;
- Other relevant geotechnical issues which may impact construction; and
- Recommendations for further geotechnical input.
- Commentary on geotechnical site suitability for the proposed works.

1.3 Published Geological Mapping

The Department of Mineral Resources Geological Map Sydney 1:100,000 Geological Series Sydney (DMR 1983) indicates the site overlies Ashfield Shale near the boundary with Hawkesbury Sandstone. Ashfield Shale generally comprises black to dark grey shale and laminite. Hawkesbury Sandstone generally comprise medium to coarse grained quartz sandstone, very minor shale and laminite lenses.

1.4 Published Soil Landscapes

The Soil Conservation Service of NSW Sydney 1:100,000 Soil Landscapes Series Sheet 9130 indicates that the residual landscape at the site likely comprises the Blacktown Landscape. This landscape type typically

includes undulating to rolling low hills on Wianamatta Group Shales with narrow ridges, hillcrests, valleys and slopes of 5 to 20 %. It generally comprises shallow to moderately deep (< 1.5 m) red and brown podzolic soils on crests and upper slopes. These soils are noted to present high soil erosion hazard, localised impermeable moderately reactive and highly plastic soil.

2 OBSERVATIONS

2.1 Investigation Methods

The original fieldwork for the site was undertaken by Morrow Geotechnics on 25 & 26 February and 1 March 2021. The additional round of borehole drilling was undertaken by Morrow Geotechnics on 3, 4 & 7 February 2022. Work carried out as part of this investigation includes:

- Review of publicly available information from previous reports in the project area, published geological and soil mapping and government agency websites;
- Site walkover inspection by a Geotechnical Engineer to assess topographical features, condition of surrounding structures and site conditions;
- Dial Before You Dig (DBYD) services search of proposed borehole locations;
- Drilling of four additional boreholes. The boreholes (BH7, BH8, BH9 and BH10) were drilled by a track
 mounted drill rig using solid flight augers equipped with a tungsten-carbide bit (TC bit). The boreholes
 were extended beyond TC bit refusal by NMLC coring techniques to depths of between 14.40 and
 15.20 mBGL. Rock core was boxed and photographed and point load tests were undertaken on
 selected core sample to assess rock strength. Borehole locations are shown on Figure 1 and borehole
 logs are presented in Appendix A;
- Measurement of water levels within monitoring wells in BH1 and BH5 drilled as part of the previous investigation.

2.2 Subsurface Conditions

The stratigraphy at the site is characterised by residual soil overlying sandstone. The observed ground conditions have been divided into five geotechnical units. A summary of the subsurface conditions at the investigation locations is presented below in **Table 1**.

TABLE 1 SUMMARY OF INFERRED SUBSURFACE CONDITIONS

	Unit	Generalised Description
1	Fill	Generally fine to medium grained sand with some silt, gravel, organic material present. Unit 1 is inferred to be uncontrolled and poorly compacted.
2	Residual Soil	Low to medium plasticity sandy clay. Stiff to hard consistency, grading to extremely weathered rock with depth.
3	Class IV Sandstone	Sandstone, highly weathered, very low to low strength.

4	Class III Sandstone	Sandstone, moderately weathered, medium to high strength. Defects within Unit 4 comprise bedding partings inclined to 30° and joints inclined up to 60°. Minor shale banding is present within Unit 4.
5	Class II Sandstone	Sandstone, slightly weathered to fresh, high strength. Defects within Unit 5 bedding partings inclined to 5° and joints inclined up to 90°.

Notes:

TABLE 2 SUMMARY OF SUBSURFACE CONDITIONS AT INVESTIGATION LOCATIONS

Material	Unit 1 Fill	Unit 2 Residual Soil	Unit 3 Class IV Sandstone	Unit 4 Class III Sandstone	Unit 5 Class II Sandstone
BH1	0.0 to 0.35	0.35 to 0.8	0.8 to 2.7	2.7 to 4.8	4.8 to 14.52
ВН3	0.0 to 0.15	-	0.15 to 7.2	-	7.2 to 14.63
BH4	0.0 to 0.7	0.7 to 2.8	2.8 to 4.0	4.0 to 8.0	8.0 to 14.50
BH5	0.0 to 0.1	-	0.1 to 5.6	5.6 to 7.8	7.8 to 14.79
ВН6	0.0 to 0.4	0.4 to 2.3	2.3 to 2.6	2.6 to 6.25	6.25 to 14.39
BH7	0.0 to 0.5	0.5 to 1.6	1.6 to 4.4	4.4 to 7.3	7.3 to 14.40
BH8	0.0 to 0.2	0.2 to 2.6	2.6 to 4.45	4.45 to 8.05	8.05 to 14.41
ВН9	0.0 to 1.0	1.0 to 3.2	3.2 to 4.9	4.9 to 6.55	6.55 to 15.20
BH10	0.0 to 0.6	0.6 to 3.5	3.5 to 5.3	5.3 to 6.0	6.0 to 14.72

2.3 Groundwater Observations

A groundwater monitoring event was carried out on 4 March 2021 and 3 February 2022. Water levels were recorded within the two monitoring wells installed in BH1 and BH5. Water level measurements were as follows:

- BH1:
 - 4 March 2021 Water depth within monitoring well 13.57 mBGL;
 - 3 February 2022 Water depth within monitoring well 12.62 mBGL;
- BH5:
 - o 4 March 2021 Water depth within monitoring well 4.42 mBGL.
 - o 3 February 2022 Water depth within monitoring well 6.06 mBGL.

The difference in water levels measured in the two monitoring wells indicates that the results are not indicative of a regional water table at the site. The water levels are inferred to represent free water within open joints in the sandstone rock mass. A regional groundwater table was not encountered at the site during either investigation.

Depths shown are based on material observed within test locations and will vary across the site. More information on the material encountered at the test locations is shown on the Borehole logs in Appendix A.

2.4 Laboratory Test Results

Four soil samples were selected for laboratory testing. A summary of test results is provided in **Table 3**.

TABLE 3 SUMMARY OF CHEMICAL LABORATORY TEST RESULTS

Sample ID	BH7 SPT1	BH8 SPT1	BH9 SPT1	BH9 SPT2
Depth	0.5m	0.5m	0.5m	1.5m
рН	5.5	6.5	6.2	5.3
Conductivity (μS/cm)	46	19.4	74.3	120
Sulfate (mg/kg)	18.5	13.2	9.1	81
Chloride (mg/kg)	20.4	22.7	31.8	16

3 RECOMMENDATIONS

3.1 Excavation Retention

Units 1 to 3 material must be supported through adequate shoring during excavation. Units 4 and 5 Sandstone may be cut vertically without temporary support provided that geotechnical inspections are undertaken during construction to ensure that isolated blocks and wedges are not present within the rock cutting. If blocks and wedges are present isolated spot bolting, shotcreting or scaling of the rock face may be required as support. Allowance for shotcreting of Unit 4 Class III Sandstone should be included within the design drawings to be removed following geotechnical inspection if unnecessary for temporary excavation support.

Shoring systems in sandstone generally comprise anchored soldier pile walls with piles socketing below bulk excavation level (BEL). Piles can be terminated within Class III Sandstone or better material above BEL provided that toe anchors are installed for lateral pile restraint. For preliminary costing purposes a four level basement in sandstone may assume 450 to 600 mm diameter soldier piles at 2 m spacing with 2 rows of anchors.

Morrow Geotechnics understands that the finite element software packages will be used for design of shoring. Drained cohesion and friction angles for input to finite element analysis have been provided in **Table 4** below.

TABLE 4 EARTH PRESSURE PARAMETERS

	Material	Unit 1 Fill	Unit 2 Residual Soil	Unit 3 Class IV Sandstone	Unit 4 Class III Sandstone	Unit 5 Class II Sandstone
Bulk	Unit Weight (kN/m³)	17	18	23	24	24
	ated Bulk Unit ight (kN/m³)	18	19	23.5	24	24
ssure	At Rest, K _o	0.53	0.58	0.43	0.43	0.38
Earth Pressure Coefficients	Passive, K _p	2.77	2.46	3.69	3.69	4.20
Eart Co	Active, K _a	0.36	0.41	0.27	0.27	0.24
Drained (kPa)	d Cohesion, c'	0	7	50	300	750
Drained Angle,	d Friction φ' (°)	28	25	32	35	38
Elastic	Modulus (MPa)	3	15	150	500	1000
Poissor	n's Ratio	0.30	0.30	0.22	0.20	0.20

¹ Unit Weight is based on visual assessment only and may vary by ±10%.

² Earth pressures are provided on the assumption that the ground behind the retaining wall is flat and drained.

In addition, design of retaining walls should consider t appropriate surcharge loading from construction equipment, vehicular traffic and neighbouring structures at finished surface level should be taken into account in the retention design. Surcharge loads on retention structures may be calculated using a rectangular stress block with an earth pressure coefficient of 0.5 applied to surcharge loads at ground surface level.

3.2 In Situ Rock Stresses

Due to the presence of high strength sandstone at relatively shallow depth the calculation of loading on shoring systems must take in situ stresses into consideration. No specific field testing has been carried out for the subject site in order to assess the in situ stress regime.

Numerous published papers exist which document the typical in situ horizontal stress values measured from projects elsewhere within the Sydney Basin. Papers by McQueen, 2004; Chan, Kotze and Stone, 2006; Chan and Stone, 2006; Macklin, McKay and Erskine, 2014; and Oliveira and Parker, 2014 have been reviewed and used to develop the in situ horizontal stress values to be adopted.

Based on published data, the orientation of the major in situ horizontal stress is typically in a NNE direction, while the minor in situ horizontal stress is in an ESE direction. In the absence of site specific testing of the stress field the principal stress direction should be taken as perpendicular to the alignment of the shoring wall under analysis. It should be noted that this is a conservative assumption which will result in higher stress relief and displacements than the actual conditions.

Bertuzzi (2014) reproduces the relationship shown in McQueen (2004) as

$$\sigma_{H} = 2.0\sigma_{V} + 2.5 \text{ MPa}$$

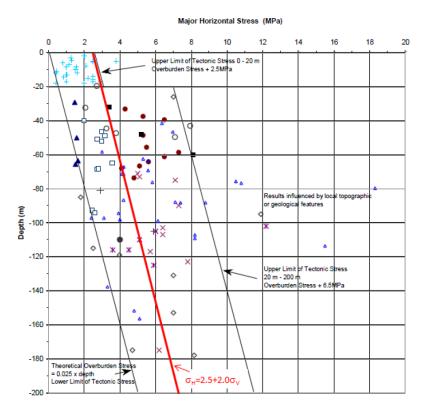


Figure 1: Plot of insitu stress to depth reproduced from McQueen (2004) and Bertuzzi (2014)

Bertuzzi's paper presents Sandstone and shale parameters for tunnel design. It is relevant to locked in stresses which can develop at depth, but not accurate for near surface effects. As can be seen from the

graph reproduced from Bertuzzi and McQueen, this overestimates the in-situ stress for shallow samples (<20 m depth) in 24 out of 25 tests. On average it produces values which are double those recorded from field testing. An upper limit of tectonic stress at σ_V + 2.5 MPa is suggested.

An in situ stress function of σ_V + 1.0 MPa encapsulates 15 of the 19 test results (approx. 80%) presented in the depth range relevant to excavation at the site. It is therefore considered a reasonable model of in situ stress conditions for modelling

The inputs to model in situ stresses for competent rock capable of maintaining locked in stress are presented in **Table 3**. These values may be used for direct input to finite element modelling software programs such as Plaxis or RS2.

TABLE 5 IN SITU STRESS RATIOS

Geotechnical Unit	Material	Typical Insitu Stress Conditions (K _{0,x})
Unit 1	Fill	-
Unit 2	Residual Soil	-
Unit 3	Class IV Sandstone	-
Unit 4	Class III Sandstone	4.0
Unit 5	Class II Sandstone	6.0

3.3 Soil and Rock Excavatability

The expected ability of equipment to excavate the soil and rock encountered at the site is summarised in **Table 6**. This assessment is based on available site investigation data and guidance on the assessment of excavatability of rock by Pettifer and Fookes (1994). The presence of medium to high strength bands in lower strength rock and the discontinuity spacing may influence the excavatability of the rock mass.

TABLE 6 SOIL AND ROCK EXCAVATABILITY

Unit	Material	Excavatability
1	Fill	Easy digging by 20t Excavator
2	Residual Soil	Easy digging by 20t Excavator
3	Class IV Sandstone	Moderate to hard ripping by 20t Excavator with hydraulic hammering required where medium strength sandstone is encountered within Unit 3
4	Class III Sandstone	Hydraulic hammering will be required in medium to high strength sandstone within Unit 4.
5	Class II Sandstone	Hydraulic hammering will be required in high strength sandstone within Unit 5.

The excavation methodology may also be affected by the following factors:

- Scale and geometry of the excavation;
- Availability of suitable construction equipment;
- Potential reuse of material on site; and
- Acceptable excavation methods, noise, ground vibration and other environmental criteria.

3.4 Excavation Vibration Considerations

As a guide, safe working distances for typical items of vibration intensive plant are listed in **Table 7**. The safe working distances are quoted for both "cosmetic" damage (refer British Standard BS 7385:1993) and human comfort (refer NSW Environmental Protection Agency Vibration Guideline). The safe working distances should be complied with at all times, unless otherwise mitigated to the satisfaction of the relevant stakeholders.

TABLE 7 RECOMMENDED SAFE WORKING DISTANCES FOR VIBRATION INTENSIVE PLANT

Plant Item	Description	Safe Working I	Distance
		Cosmetic Damage (BS 7385:1993) ¹	Human Response (EPA Vibration Guideline)
Vibratory Roller	< 50 kN (typically 1-2 tonnes)	5 m	15 m to 20 m
	< 100 kN (typically 2-4 tonnes)	6 m	20 m
	< 200 kN (typically 4-6 tonnes)	12 m	40 m
	< 300 kN (typically 7-13 tonnes)	15 m	100 m
	< 300 kN (typically 13-18 tonnes)	20 m	100 m
	< 300 kN (typically >18 tonnes)	25 m	100 m
Small Hydraulic Hammer	300 kg – 5 to 12 t excavator	2 m	7 m
Medium Hydraulic Hammer	900 kg – 12 to 18 t excavator	7 m	23 m
Large Hydraulic Hammer	1600 kg – 18 to 34 t excavator	22 m	73 m
Vibratory Pile Driver	Sheet Piles	2 m to 20 m	20 m
Pile Boring	≤ 800 mm	2m (nominal)	N/A
Jackhammer	Hand held	1 m (nominal)	Avoid contact with structure

Notes:

The safe working distances in **Table 7** relate to continuous vibration and apply to residential receivers. For most construction activities, vibration emissions are intermittent in nature and for this reason, higher vibration levels, occurring over shorter periods are permitted, as discussed in British Standard BS 6472-1:2008.

The safe working distances provided in **Table 7** are given for guidance only. Monitoring of vibration levels may be required to ensure vibrations levels remain below threshold values during the construction period. Monitoring thresholds should be set at a peak particle velocity (ppv) of 5 mm/sec to prevent structural

damage to neighbouring structures and infrastructure. Cosmetic damage to brittle elements of a structure such as tiling or plaster may occur at any vibration level. Where ppv thresholds are exceeded an alternative excavation methodology should be developed in collaboration with the geotechnical engineer to reduce the likelihood of vibration induced damage.

3.5 Groundwater Management

The wells installed as part of this investigation did not show a regional groundwater table. The proposed basement will not intersect the groundwater table and ongoing seepage will be minor. For excavations at the site it should be expected that minor seepage water from surface water infiltration will be encountered at the soil/rock interface and in joints and bedding partings within the bedrock. Seepage in sandstone bedrock may be assumed as typically flowing downwards toward local drainage lines or regional water table, along horizontal bedding planes and sub-vertical joints. The rock mass permeability will be governed by the joints, faults and bedding planes.

Given the observed relatively intact bedrock with tight defects across the site it is anticipated that the permeability of the sandstone will be relatively low and that seepage inflows will be controlled by sump and pump methods.

3.6 Foundation Design

The parameters given in **Table 8** may be used for the design of pad footings and bored piles. Morrow Geotechnics recommends that a Preliminary Geotechnical Strength Reduction Factor (GSRF) of 0.4 is used for the design of piles in accordance with AS 2159:2009 if no allowance is made for pile testing during construction. Should pile testing be nominated, the GSRF may be reviewed and a value of 0.55 to 0.65 may be expected.

Ultimate geotechnical strengths are provided for use in limit state design. Allowable bearing pressures are provide for serviceability checks. These values have been determined to limit settlements to an acceptable level for conventional building structures, typically less than 1% of the minimum footing dimension.

TABLE 8 PAD FOOTING AND PILE DESIGN PARAMETERS

Material	Unit 1 Fill	Unit 2 Residual Soil	Unit 3 Class IV Sandstone	Unit 4 Class III Sandstone	Unit 5 Class II Sandstone
Allowable Bearing Pressure (kPa)	0	200	1500	3500	6000
Ultimate Vertical End Bearing Pressure (kPa)	0	600	4500	10500	18000
Elastic Modulus (MPa)	3	15	150	400	1000
Ultimate In Shaft Compression Adhesion	n 0	50	250	800	1500
(kPa) In Tension	0	25	125	400	750
Susceptibility to Liquefaction during an Earthquake	Medium	Low	Low	Low	Low

Notes:

1 Side adhesion values given assume there is intimate contact between the pile and foundation material. Design engineer to check both 'piston' pull-out and 'cone' pull-out mechanics in accordance with AS4678-2002 Earth Retaining Structures.

2 Susceptibility to liquefaction during an earthquake is based on the following definition:

Low - Medium to very dense sands, stiff to hard clays, and rock

Medium - Loose to medium dense sands, soft to firm clays, or uncontrolled fill below the water table

High - Very loose sands or very soft clays below the water table

To adopt these parameters we have assumed that the bases of all pile excavations are cleaned of loose debris and water and inspected by a suitably qualified Geotechnical Engineer prior to pile construction to verify that ground conditions meet design assumptions. Where groundwater ingress is encountered during pile excavation, concrete is to be placed as soon as possible upon completion of pile excavation. Pile excavations should be pumped dry of water prior to pouring concrete, or alternatively a tremmie system could be used.

If Unit 5 Class II Sandstone parameters are relied on for footing design it will be necessary to carry out spoon testing on a minimum of 50% of the footings to confirm rock quality. Spoon tests should be carried out to a depth of at least two times the minimum footing width below the proposed footing level.

Selection of footing types and founding depth will need to consider the risk of adverse differential ground movements within the foundation footprint and between high level and deeper footings. Unless an allowance for such movement is included in the design of the proposed development we recommend that all new structures found on natural materials with comparable end bearing capacities and elastic moduli.

3.7 AS1170 Earthquake Site Risk Classification

Assessment of the material encountered during the investigation in accordance with the guidelines provided in AS1170.4-2007 indicates:

- an earthquake subsoil class of Class B_e Rock for the site; and
- a hazard factor (z) of 0.08 for Sydney.

3.8 Soil Aggressivity

Analysis of the pH, chloride & sulfate content and electrical conductivity of the soil against the guidelines provided in AS2159-2009 indicates:

- 'mildly aggressive' to buried concrete structural elements; and
- 'mildly aggressive' to buried steel structural elements.

Laboratory test certificates for aggressivity testing are included in Appendix B.

4 RECOMMENDATIONS FOR FURTHER GEOTECHNICAL SERVICES

Further input from a geotechnical professional during design and construction is advised in order to ensure a cost-effective design which can be constructed safely and efficiently. Areas for geotechnical input should include:

- A suitably qualified geotechnical engineer is to assess the condition of exposed material at foundation or subgrade level to assess the ability of the prepared surface to act as a foundation or as a subgrade.
- Regular inspections of battered and unsupported excavations, where proposed, to confirm
 geotechnical conditions and to assess the suitability of design assumptions and to provide further
 advice with regards to excavation retention/ support and proposed construction methodologies,
 if required.

5 CONCLUSION

Site conditions encountered in the investigation are generally consistent with regional Sydney Geology. The site is geotechnically suitable for development and excavation may be carried out safely provided that the recommendations of this report are implemented in design and construction of the works.

6 STATEMENT OF LIMITATIONS

The adopted investigation scope was limited by the investigation intent. Further geotechnical inspections should be carried out during construction to confirm both the geotechnical model and the design parameters provided in this report.

Your attention is drawn to the document "Important Information", which is included in **Appendix B** of this report. The statements presented in this document are intended to advise you of what your realistic expectations of this report should be. The document is not intended to reduce the level of responsibility accepted by Morrow Geotechnics, but rather to ensure that all parties who may rely on this report are aware of the responsibilities each assumes in so doing.

7 REFERENCES

AS1726:1993, Geotechnical Site Investigations, Standards Australia.

AS2159:2009, Piling – Design and Installation, Standards Australia.

AS2870:2011, Residential Slabs and Footings, Standards Australia.

AS3798:2007, *Guidelines on Earthworks for Commercial and Residential Developments*, Standards Australia.

NSW Department of Finance and Service, Spatial Information Viewer, maps.six.nsw.gov.au.

Pells (2004) Substance and Mass Properties for the Design of Engineering Structures in the Hawkesbury Sandstone, Australian Geomechanics Journal, Vol 39 No 3

8 CLOSURE

Please do not hesitate to contact Morrow Geotechnics if you have any questions about the contents of this report.

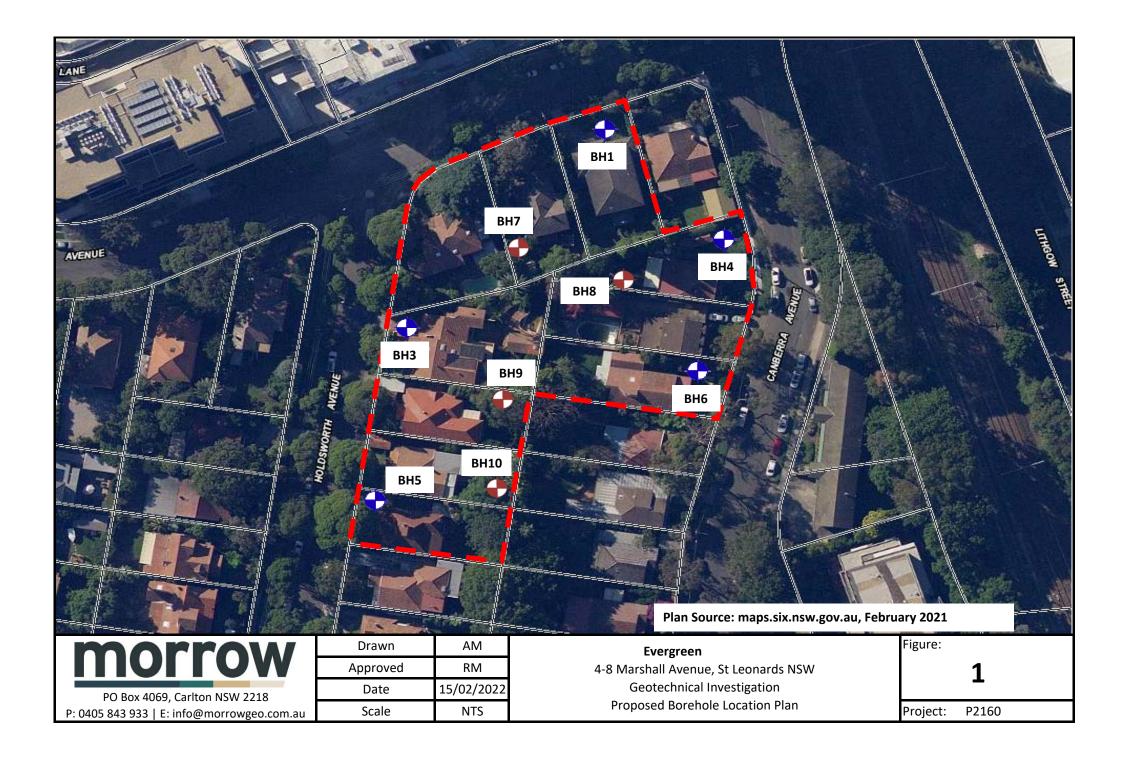
For and on behalf of Morrow Geotechnics Pty Ltd,

Alan Morrow

Principal Geotechnical Engineer

P2160 01 16/02/2022

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BOREHOLE LOGS

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



BH1 Hole ID.

Hole Depth: 14.52 m

1 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 25-FEB-21 Ground Level: Drill Method: **SFA/NLMC** Date Completed: 25-FEB-21 Easting:

Equipment: Track mounted Hanjin Drill Rig Northing:

Samples Samples Tests Observations Samples Tests Set Tests	
Silty SAND- dark brown, fine to medium grained, roots. Sandy CLAY- orange brown, fine to medium grained. Stiff m	s / Comments
Silty SAND- dark brown, fine to medium grained, roots. Sandy CLAY- orange brown, fine to medium grained. Stiff m	
SANDSTONE- orange yellow, medium grained, extremely to highly weathered, estimated very low strength. Sandstone orange yellow, medium grained, extremely to highly weathered, estimated low strength.	
SANDSTONE- orange yellow, medium grained, extremely to highly weathered, estimated very low strength. N=15 Description: N=15 N=15 Description: N=15 Description: N=15 Description: N=15 Description: N=15 Description: N=15 N=15 Description: N=15 Descr	
- :::	
- :::: BH1 continued as cored hole from 2.5m	
Moisture Additional Comments D Dry	
Dp Damp SM Slightly Moist M Moist VM Very Moist W Wet Sd Saturated	
Logged By: Matthew Kilham Date: 25-Feb-21 Checked By: Alan Morrow Date:	

٩_			
<u> </u>	Mois	ture	Additional Comments
₽-	D	Dry	
	Dp	Damp	
9	SM	Slightly Moist	
\subseteq	M	Moist	
픘	VM	Very Moist	
S	W	Wet	
<u> </u>	Sd	Saturated	
₹-			

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933

SFA/NLMC

Drill Method:



BH1 Hole ID.

Hole Depth: 14.52 m

2 of 4 Sheet:

Easting:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Date Completed:

25-FEB-21

Drilling Company: **BG** Drilling Date Started: 25-FEB-21 Ground Level:

Equipment: Track mounted Hanjin Drill Rig Northing:

SANDSTONE - grey white orange and purple, medium to coarse grained, weak to moderate iron staining, trace carbonaceous laminations. SANDSTONE - grey white orange and purple, medium to coarse grained, weak to moderate iron staining, trace carbonaceous laminations. Amount of the coarse grained, weak to moderate iron staining, trace carbonaceous laminations. Additional Comments Matthew Kilham Date: 25-Feb-21 Checked By: Alan Morrow Date: 07-MAR-21

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SFA/NLMC

Drill Method:



BH1 Hole ID.

Hole Depth: 14.52 m

3 of 4 Sheet:

Easting:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Date Completed:

25-FEB-21

Drilling Company: **BG** Drilling Date Started: 25-FEB-21 Ground Level:

Equipment: Track mounted Hanjin Drill Rig Northing:

Method Water Level Depth (m)	KL (m) Graphic Log	Material Type	Material Description	Weathering	Estimated Strength (MPa)	D=diametral M Ø A=axial & Ø (6)	U.C.S. (Mpa)	RQD %	Core Photo	Defect Spacing (mm)	Defect Description type, inclination, thickness, shape,	Depth (m)	Casing & Core Lifts
		Bedrock	SANDSTONE - grey white some orange, medium to coarse grained, weak iron staining, trace carbonaceous laminations. SANDSTONE - grey white, medium to coarse grained, trace carbonaceous laminations.	SW-FR	× × × × × × × × × × × × × × × × × × ×	A=0.85 D=0.73 A=1.99 D=1.44 A=2.34 D=1.35 A=0.16 D=0.21 A=1.22 D=1.22		98 84 84			— HB — HB — Bd, 5, clay infill 2mm Bd, 5, clay infill 2mm SM, 0, clay 10mm — HB — BD, 1, FE, RG — BB, 5, Clay 10mm — HB — HB — HB — HB — HB — DB, 5, clay infill 1mm — SM, 0, clay, 100mm		11.5
Additional	Comme	ents											

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



BH1 Hole ID.

Hole Depth: 14.52 m

4 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 25-FEB-21 Ground Level:

Drill Method: **SFA/NLMC** Date Completed: 25-FEB-21 Easting: Equipment: Track mounted Hanjin Drill Rig Northing:

Method Water Level Depth (m) RL (m)	Graphic Log Material Type	Material Description	Weathering	Estimated Strength (MPa) MPa MPa		ROD % Core Photo	Defect Spacing (mm)	Defect Description type, inclination, thickness, shape, roughness, coating Specific General	Depth (m)	Casing & Core Lifts
MINO DE LEGRA DE LEGR	Gr. Bedrock Ma	SANDSTONE - grey white, medium to coarse grained, trace carbonaceous laminations. Hole Terminated at 14.52 m Target depth achieved	FR FR		5.59	N		—Bd, 0, FE, RG □-SM, 5, clay, 50mm	12.5 - 13.5 - 14.0 - 15.0 - 16.5 - 17.0 - 17.5 - 17.5 - 18.0	14.52
Additional Co	omments	;								



Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



BH3 Hole ID.

Hole Depth: 14.63 m

Sheet: 1 of 4

Project Number: P2160 Project Name: **Geotechnical Assessment**

Location / Site: 4-8 Marshall Street, St Leonards NSW Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 01-MAR-21 Ground Level: Drill Method: **SFA/NLMC** 01-MAR-21 Date Completed: Easting: Northing: Equipment: Track mounted Hanjin Drill Rig

USCS Symbol Material Type Water Level Graphic Log Ξ Material Description Observations / Comments Depth ($\widehat{\Xi}$ 퓝 Surface: Paver/Concrete slab PAVER/CONCRETE. SANDSTONE with bands Sandy CLAY- red yellow, extremely to highly weathered with bands residual sandy clay, estimated very low strength. 1.0 Bedrock SFA 2.0 becoming orange yellow. predominatly grey. 3.0 BH3 continued as cored hole from 2.9m 4.0 5.0

DAVIES BH LOG DRAFT LOGS ST LEONARDS.GPJ GEE.GDT 7-3-21 12:05:04 PM Moisture Damp Slightly Moist M VM Moist Very Moist W Wet Sd

Additional Comments

Matthew Kilham Date: 01-Mar-21 Logged By: Checked By: **Alan Morrow** Date: 07-MAR-21 Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



Hole ID.

14.63 m

BH3

Hole Depth: Sheet:

P2160

2 of 4

Project Name: **Geotechnical Assessment** Project Number:

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 01-MAR-21 Ground Level: Drill Method: **SFA/NLMC** Date Completed: 01-MAR-21 Easting:

Northing: Equipment: Track mounted Hanjin Drill Rig

									Γ.		R	ock N	lass Defe	erts		\Box
Method Water Level	Depth (m)	RL (m)	Graphic Log	Material Type	Material Description	Weathering	Estim Strer (MF	ngth Pa)	D=diametral M signal A=axial B (G)	U.C.S. (Mpa)	RQD %	Core Photo	Defect Spacing (mm)	Defect Description type, inclination, thickness, shape, roughness, coating Specific General	Depth (m)	Casing & Core Lifts
STLEONARDS.GPJ GEE.GDT 7-3-21 12:05:27 PM NLMC				Bedrock	SANDSTONE - white purple orange, medium to coarse grained, moderate iron staining. SANDSTONE - grey white some orange, fine to medium grained. SANDSTONE - grey and orange, fine to medium grained, weakly iron stained. SANDSTONE - light grey and grey, fine to medium grained, trace carbonaceous laminations.	RS XW-DW	**		A=0.08 D=0.03 A=0.44 D=0.6		N			Specific General Specific General JT, 70, clay, 40mm JT, 70, clay infill SM, 0, clay, 30mm SM, 0, clay, 10mm SM, 0, clay, 50mm HB BD, 1, clay infill 2mm, SMTH BD, 9, clay infill 2mm, SMTH SMTH SMTH BD, 5, clay infill 2mm, SMTH BD, 4, clay infill 2mm, SMTH SMTH DB BD, 3, clay infill 2mm, SMTH	al	5.64
GEE DAVIES C	Lo	gged	d By:		Matthew Kilham Date: 01-Mar-21			Che	cked E	Зу:	Al	an M	orrow	Date: 07-MAR-	21	<u> </u>

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933

Location / Site:

Drill Method:

Drilling Company:



Hole ID.

BH3 14.63 m

3 of 4

Hole Depth:

Sheet:

P2160

Project Name: **Geotechnical Assessment**

4-8 Marshall Street, St Leonards NSW

Project Number:

Client: **Evergreen Investment Holdings**

BG Drilling Date Started: **SFA/NLMC** Date Completed:

01-MAR-21 01-MAR-21

Easting:

Ground Level:

Equipment: Track mounted Hanjin Drill Rig Northing:

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



Hole ID.

BH3

Hole Depth:

Sheet:

14.63 m 4 of 4

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 01-MAR-21 Ground Level: Drill Method: **SFA/NLMC** Date Completed: 01-MAR-21 Easting:

Equipment: Track mounted Hanjin Drill Rig Northing:

pc	Water Level	Depth (m)	(1	Graphic Log	Material Type	Material Description	Weathering	Estimated Strength (MPa)	D=diametral த <i>ு</i> A=axial ^ற ்	s. (Mpa)		Core Photo A 30	Defect Spacing (mm)	cts Defect Description type, inclination, thickness, shape, roughness, coating	(m) r	Casing &
Method	Wate	Dept	RL (m)	Grap	Mate		Weal	EL 0.03 N	D=dia A=axi	U.C.S.	RQD %	Core	20 80 200 2000	Specific General	Depth (m)	Casi
		12.5				SANDSTONE - grey white, medium to coarse grained, trace carbonaceous laminations.	FR		A=1.92 D=1.89					—BD, 5 , FE, RG	- - 12.5 - - - 13.0	
NLMC		13.5			Bedrock				A=2.51 D=2.04 A=1.45 D=1.38		100			—BD, 5 , FE, RG	13.5	
		14.5 - - - - - - - - - - - - - - - - - - -				Hole Terminated at 14.63 m Target depth achieved								—BD, 5 , FE, RG	14.5 - 15.0 - 15.5 - 16.0 - 17.0	14.6.55
	Add	18.0	al Co	ommo	ents										18.0	



1 of 4

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



BH4 Hole ID.

Hole Depth: 14.50 m

Sheet:

Project Number: P2160 Project Name: **Geotechnical Assessment**

Location / Site: 4-8 Marshall Street, St Leonards NSW Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 25-FEB-21 Ground Level: Drill Method: **SFA/NLMC** 25-FEB-21 Date Completed: Easting: Northing: Equipment: Track mounted Hanjin Drill Rig

amples Tests USCS Symbol Material Type Consistency / Density Water Level Graphic Log Ξ Material Description Observations / Comments Moisture RL (m) Depth (SPT FILL: Silty Sandy CLAY- dark brown, low plasticity, fine to m CL firm to stiff Sandy CLAY- orange brown, low plasticity, fine to medium 2 N=3 grained. 1.0 SFA Residual Soil 3 N=7 2.0 SANDSTONE bands Sandy CLAY- grey purple, fine to 3.0 coarse grained. BH4 continued as cored hole from 3.05m 4.0 5.0

DAVIES BH LOG DRAFT LOGS ST LEONARDS.GPJ GEE.GDT 7-3-21 12:05:05 PM Moisture Damp Slightly Moist Moist Very Moist W Wet Sd

Additional Comments

Matthew Kilham Date: 25-Feb-21 Logged By: Checked By: **Alan Morrow** Date: 07-MAR-21

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



BH4 Hole ID.

Hole Depth: 14.50 m

2 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 25-FEB-21 Ground Level: Drill Method: **SFA/NLMC** Date Completed: 25-FEB-21 Easting:

Northing: Equipment: Track mounted Hanjin Drill Rig

Ī				6	ed			Estimated Strength (MPa)	Is ₍₅₀₎ MPa	oa)	R		lass Defe	Defect Description		$\overline{\square}$
Mothor Codt	Water Level	Depth (m)	RL (m)	Graphic Log	Material Type	Material Description	Weathering	13 1 33 1 50 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	D=diametral A=axial	U.C.S. (Mpa)	RQD %	Core Photo	Spacing (mm)	type, inclination, thickness, shape, roughness, coating Specific Gene	ral Depth (m)	Casing & Core Lifts
																;
ARDS.GPJ GEE.GDT 7-3-21 12:05:31 PM		3.5			Bedrock	Sandy CLAY - grey purple, low plasticity, fine to coarse grained. SANDSTONE - grey white, fine to coarse grained, trace carbonaceous laminations. SANDSTONE - purple, fine to coarse grained, moderate iron staining. SANDSTONE - grey white, fine to coarse grained.	RS DW	о «	A=0.8 A=1.14 D=1.57		98	× × ×		□-SM, 0, clay, 10mm —BD, 0, FE, RG —ironstone band —BD, 0, FE, RG	3.5. 	
GEE DAVIES CH LOG DRAFT LOGS ST LEONARDS.GPJ	Add	6.0	al C	omm	ents						94				6.0	
GEE DAN		Lo	oggeo	d By:		Matthew Kilham Date: 25-Feb-21		Che	ecked I	By:	Ala	an M	orrow	Date: 07-MAF	2-21	

BH4

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933

Drill Method:



Hole ID.

Easting:

Hole Depth: 14.50 m

3 of 4 Sheet:

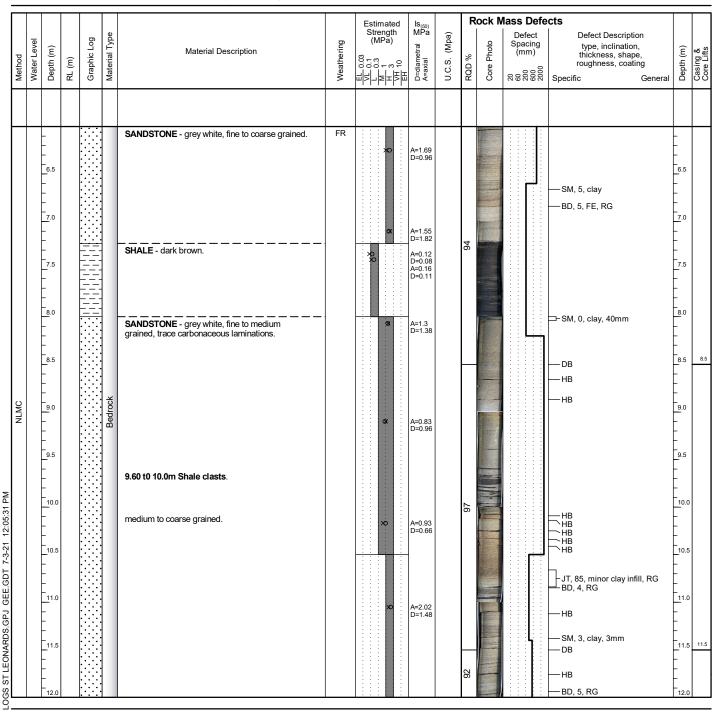
P2160 Project Name: **Geotechnical Assessment** Project Number:

Location / Site: 4-8 Marshall Street, St Leonards NSW Client: **Evergreen Investment Holdings**

Date Completed:

Drilling Company: **BG** Drilling Date Started: 25-FEB-21 Ground Level: **SFA/NLMC** 25-FEB-21

Northing: Equipment: Track mounted Hanjin Drill Rig



Additional Comments

DAVIES CH LOG DRAFT

Matthew Kilham Logged By: Date: 25-Feb-21 Checked By: **Alan Morrow** Date: 07-MAR-21

BH4

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933

SFA/NLMC

Drill Method:



Hole ID.

Easting:

Hole Depth: 14.50 m

4 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

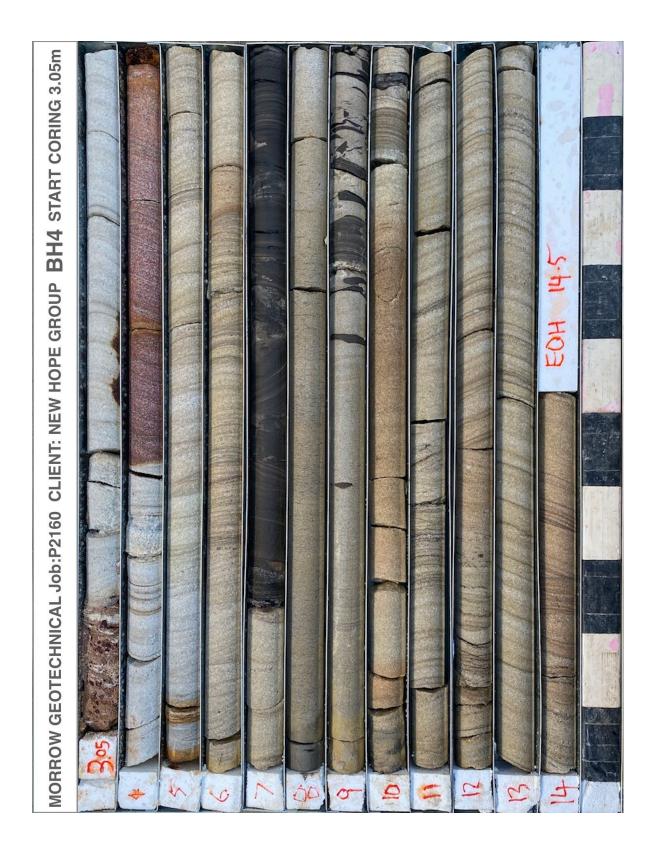
Date Completed:

25-FEB-21

Drilling Company: **BG** Drilling Date Started: 25-FEB-21 Ground Level:

Equipment: Track mounted Hanjin Drill Rig Northing:

Aethod Vater Level	'L (m)	sraphic Log	faterial Type	Material Description	Veathering	Estimated Strength (MPa)	axial DG®	J.C.S. (Mpa)			Defect Spacing (mm)	Defect Description type, inclination, thickness, shape,	Jepth (m)	asing &
NLMC Method Mater Level Mater Level Method Mater Level	3.5	Graphic Log	Bedrock Material Type	SANDSTONE - grey white, fine to medium grained, trace carbonaceous laminations. Hole Terminated at 14.50 m Target depth achieved	出 Weathering		<u>a</u>	U.C.S. (Mpa)	92 RQD %	Core Photo	Defect Spacing (mm)	type, inclination, thickness, shape,	(E) Hided	14.
	7.5	Comm	ents										16.0 	



Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



BH5 Hole ID.

Hole Depth: 14.79 m

1 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 26-FEB-21 Ground Level: Drill Method: **SFA/NLMC** Date Completed: 25-FEB-21 Easting:

Equipment: Track mounted Hanjin Drill Rig Northing:

									Ī
Method Water Level	Depth (m)	RL (m)	Graphic Log	USCS Symbol	Material Type	Material Description	Observations / Comments	Well Details	
						Surface: Concrete			
	-		p. 5. 3			CONCRETE.	0.00 0.10 0.15	ě	į.
	-					SANDSTONE with clay seams- grey orange, fine to coarse grained, extremely to highly weathered, estimated very low to low strength.			
	_ 1.0						400		
	-						1.00		
¥10	_				ock				
ס	-				Bedrock				
	2.0								
	-								
	-								
	-						2.80m drilling becoming firm		
	3.0					BH5 continued as cored hole from 3m	2.80m drilling becoming firm to hard		:
	-					Bris Continued as cored note from Sin			
	-								
	-								
	<u>4</u> .0								
	-								
	-								
	-								
	5.0								
	_								
	-								
	-								
Mois	6.0					Additional Comments			
D Dp	Dry Dar					Additional Comments			
SM M	Sligl Moi	htly M st							
VM W Sd	Wet	y Mois t urated							

٩_			
Ĕ_	Mois	ture	Additional Comments
₽-	D	Dry	
DR	Dp	Damp	
90	SM	Slightly Moist	
_	M	Moist	
H	VM	Very Moist	
S	W	Wet	
IES	Sd	Saturated	
₹-			

BH5

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933

SFA/NLMC

Drill Method:



Hole ID.

Easting:

Hole Depth: 14.79 m

2 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Date Completed:

25-FEB-21

Drilling Company: **BG** Drilling Date Started: 26-FEB-21 Ground Level:

Northing: Equipment: Track mounted Hanjin Drill Rig

Method	Water Level	Depth (m)	RL (m)	Graphic Log	Material Type	Material Description	Weathering	Estimated Strength (MPa)	D=diametral M $\overline{\omega}$ A=axial $\overline{\omega}$	U.C.S. (Mpa)	RQD %	Core Photo	Defect Spacing (mm)	Defect Description type, inclination, thickness, shape, roughness, coating Specific General		Well Details	Depth (m)	Casing & Core Lifts
GEE DAVIES CH LOG DRAFT LOGS ST LEONARDS.GPJ GEE.GDT 7-3-21 12:05:36 PM NLMC			al Co	omme	Bedrock	white orange, fine to medium grained, weak iron staining.	DW-SW	×	A=0.38 D=0.22		92 94 94			BD, 1, RG BD, 3, RG BD, 15, RG BD, 15, RG BD, 10, RG BD, 0, clay 20mi SM, 0, clay 20mi SM, 0, clay 20mi SM, 0, clay 20mi SM, 0, clay 20mi	n n n			5.68
GEE DA		Lo	gged	d By:	I	Matthew Kilham Date: 26-Feb-21		Che	ecked I	Ву:	Al	an M	orrow	Date:	07-N	IAR-2	1	<u> </u>

BH₅

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933

Drill Method:

SFA/NLMC



Hole ID.

Easting:

Hole Depth: 14.79 m

Sheet: 3 of 4

Project Name: Geotechnical Assessment Project Number: P2160

Location / Site: 4-8 Marshall Street, St Leonards NSW Client: Evergreen Investment Holdings

Drilling Company: BG Drilling Date Started: 26-FEB-21 Ground Level: ------

Equipment: Track mounted Hanjin Drill Rig Northing: ------

Date Completed:

25-FEB-21

Rock Mass Defects Estimated Is₍₅₀₎ MPa Strength (MPa) (Мра) Defect Defect Description Material Type Spacing (mm) Water Level type, inclination, thickness, shape, roughness, coating Weathering Core Photo Casing & Core Lifts Ξ Material Description Depth (m) Graphic L D=diametra A=axial Method $\widehat{\Xi}$ U.C.S. Depth (R Well 퓝 88888 Specific General BD, 2, RG BD, 0, RG DW-SW BD, 0, RG SANDSTONE - grey white orange, fine to coarse SW-FR 6.5 6.5 grained, weak iron staining, trace carbonaceous A=1.71 D=1.47 -SM, 0, clay 20mm `HB 7.0 7.0 A=2.3 D=0.46 A=2.02 BD, 1, RG 92 7.5 7.5 BD, 5, RG SM, 0, clay 5mm T8.0 8.0 A=2.6 D=2.58 SANDSTONE - grey white, fine to coarse grained, trace carbonaceous laminations. FR 8.5 8.5 8.57 DB BD, 2, SMTH Bedrock 9.0 9.0 A=1.44 D=1.3 T_{9.5} 9.5 7-3-21 12:05:36 PM √BD, 1, RG √HB T10.0 10.0 A=2.06 D=1.85 66 -BD, 3, RG 10.5 10.5 ST LEONARDS.GPJ GEE.GDT 11.0 11.0 BD, 1, SMTH SHALE/SILTSTONE - dark brown grey. FR SM, 0, clay 10mm BD, 10, SMTH A=0.4 D=0.43 T11.5 ·BD, 5, RG ·BD, 5, SMTH SANDSTONE - grey white, fine to coarse grained, SW-FR weak iron staining, trace carbonaceous laminations LOGS

Additional Comments

DAVIES CH LOG DRAFT

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933

SFA/NLMC

Drill Method:



Hole ID.

Easting:

Sheet:

25-FEB-21

BH5

4 of 4

Hole Depth: 14.79 m

Project Name: **Geotechnical Assessment** Project Number: P2160

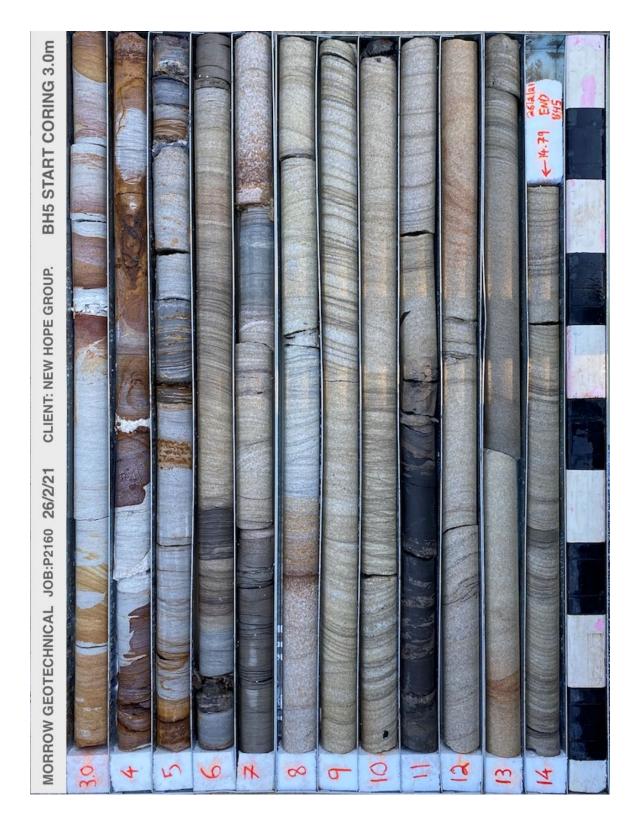
4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Date Completed:

Drilling Company: **BG** Drilling Date Started: 26-FEB-21 Ground Level:

Equipment: Track mounted Hanjin Drill Rig Northing:

	le/			go.	-ype		Đ.	Estimated Strength (MPa)	Is ₍₅₀₎ MPa	(Mpa)	R		Defect	cts Defect Description type, inclination.		siis		_
Method	Water Level	Depth (m)	RL (m)	Graphic Log	Material Type	Material Description	Weathering	四 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日	D=diametral A=axial	U.C.S. (N	RQD %	Core Photo	Spacing (mm)	thickness, shape roughness, coatir Specific Gener	i, ig	Well Details	Depth (m)	Casing &
									A-2 56									
		- - -				SANDSTONE - grey white, fine to coarse grained, weak iron staining, trace carbonaceous laminations.	SW-FR		A=2.56 D=2.71					—BD, 5, RG			·	
		12.5 			:									SM, 0, clay 5m SM, 0, clay 5m	m m		12.5	
		13.0						· · · · ∞	A=1.41 D=1.9								13.0	
NLMC		_ 13.5 			Bedrock						88	-		— НВ			13.5	
		14.0			· ·									— НВ — НВ			- - 14.0	
		-			:)XO	A=1.68 D=1.52					TID			-	
		_14.5 _ _ _												— нв	14.75		- 14.5	14
		15.0				Hole Terminated at 14.79 m Target depth achieved											15.0	
		_ 15.5															15.5	
		16.0															16.0	
		-																
		_16.5 _ _ _															16.5	
		17.0																
		_ 17.5															17.5	
		_ _ _ 18.0															18.0	
Α	∖dd	ition	al Co	omm	ents													
_		10	naer	d By:		Matthew Kilham Date: 26-Feb-21	1	Cho	cked I	Rv.	ΛI	an M	orrow	Data	07-M	ΔR_21		_



BH6

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



Hole ID.

Hole Depth: 14.39 m

1 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 26-FEB-21 Ground Level: Drill Method: **SFA/NLMC** Date Completed: 25-FEB-21 Easting:

Equipment: Track mounted Hanjin Drill Rig Northing:

	_qu	ірпіє	71 IL.			110	ack mounted Hanjin Drill Rig				1101 ti iii ig
Method	Water Level	Depth (m)	RL (m)	Graphic Log	USCS Symbol	Material Type	Material Description	Consistency / Density	Moisture	Samples / Tests SPT	Observations / Comments
_							Surface: Lawn TOPSOIL: Sandy SILT- dark brown, trace fine Gravel,		m to w		
		-			ML		roots.				
		Ė					Silty CLAY- orange brown, medium to high plasticty.	stiff		3	
		_					becoming orange mottled grey.			5 6	
		1.0			СН		becoming grey mottled red and orange.			N=11	
4		F				Soil					
SFA		Ē		//		Residual Soil	Sandy CLAY- grey some red, low plasticity, fine to coarse	stiff	m		
		_				Re	grained.			4 5	
		2.0			CL					7 N=12	
		Ē.									
		E				Joc.	SANDSTONE- orange grey, fine to coarse grained,				
<u> </u>		_				Bedrock	extremely to highly weathered, estimated very low to low strength.				
		Ē					BH6 continued as cored hole from 2.6m				
		3.0									
		-									
		_									
		L									
		4.0									
		ļ.									
		5.0									
		_									
		-									
		-									
		-									
		6.0									
	Moi:	sture Dry					Additional Comments				
5	Op SM	Dai Slig	mp Ihtly M	loist							
١	M ∕M N	Mo Ver We	y Moi	st							
	Sd		urated	d							
		Lo	gged	d By:	ı	Vlat	thew Kilham Date: 26-Feb-21 Cr	necked By:	Alan	Morro	w Date: 07-MAR-21
_											

Moisture	Additional Comments
D Dry Dp Damp SM Slightly Moist M Moist VM Very Moist W Wet Sd Saturated	

Borehole Log Report

BH6

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933



Hole ID.

Hole Depth: 14.39 m

2 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Drilling Company: **BG** Drilling Date Started: 26-FEB-21 Ground Level: Drill Method: **SFA/NLMC** Date Completed: 25-FEB-21 Easting:

Northing: Equipment: Track mounted Hanjin Drill Rig

Method	Water Level	Depth (m)	RL (m)	Graphic Log	Material Type	Material Description	Weathering	S	stimated strength (MPa)	!	D=diametral M or A=axial b (6)	U.C.S. (Mpa)	RQD %	Core Photo	Defect Spacing (mm)	Defect Dese type, inclir thickness,		Depth (m)	Casing & Core Lifts
DAVIES CH LOG BRAFT LOGS ST LEONARDS.GPJ GEE.GDT 7:3-21 12:05:40 PM NLMC	Add		al Co	omme	Bedrock	SANDSTONE - purple grey, fine to coarse grained, weak to moderate iron staining, trace carbonaceous laminations. SANDSTONE - grey some orange, fine to medium grained, weak iron staining, trace carbonaceous laminations.	DW-SW	V	100 (X	AD AD	=2.16 =1.99 =1.18 =1.36 =0.65 =0.65		94 100			BD, 10, RG BD, 15, RG SM, 0, clay 20m SM, 0, clay 5mn BD, 10, SMTH BD, 8, SMTH HB BD, 15, SMTH BD, 2, SMTH BD, 2, SMTH BD, 2, SMTH BD, 15, SMTH BD, 5, RG BD, 5, RG BD, 5, RG BD, 5, RG BD, 4, RG	m		5.43
GEE DAVIES		Lo	ggeo	d By:		Matthew Kilham Date: 26-Feb-21		T	Cl	necl	ked E	By:	Al	an M	orrow	Date:	07-MAR-2	1	

Borehole Log Report

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933

SFA/NLMC

Drill Method:



Hole ID.

Easting:

BH6

Hole Depth: 14.39 m

3 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Date Completed:

25-FEB-21

Drilling Company: **BG** Drilling Date Started: 26-FEB-21 Ground Level:

Northing: Equipment: Track mounted Hanjin Drill Rig

Method	Water Level	Depth (m)	RL (m)	Graphic Log	Material Type	Material Description	Weathering	Estimated Strength (MPa)	D=diametral M & A=axial & & & & & & & & & & & & & & & & & & &	U.C.S. (Mpa)	RQD %	Core Photo	Defect Spacing (mm)	Defect Description type, inclination, thickness, shape,	Depth (m)	Casing & Core Lifts
GEE DAVIES CH LOG DRAFT LOGS ST LEONARDS.GPJ GEE.GDT 7-3-21 12:05:40 PM NLMC	Add				ents	SANDSTONE - grey some orange, fine to medium grained, weak iron staining, trace carbonaceous laminations. SANDSTONE - grey, fine to coarse grained, trace carbonaceous laminations.	SW-FR	30 CX	A=1.36 D=1.21 A=1.9 D=2.5 A=2.28 A=2.17 D=2.08		100 93 94			SM, 0, clay 30mm SM, 0, clay 10mm SM, 0, clay 10mm BM, 0, clay 10mm BD, 2, SMTH HB BD, 10, SMTH BD, 10, RG SM, 0, clay 20mm DB BD, 10, RG BD, 5, RG BD, 3, RG BD, 3, RG BD, 4, RG BD, 4, RG BD, 4, RG BD, 10, RG BD, 10, RG BD, 10, RG BD, 10, RG BD, 3, RG BM, 0, clay 10mm BD, 5, RG BD, 10, RG BD, 3, RG		11.47
GEE D		Lo	gged	d By:		Matthew Kilham Date: 26-Feb-21		Che	cked I	Зу:	Al	an M	orrow	Date: 07-MAR-2	1	

Borehole Log Report

Morrow Geotechnics Pty Ltd PO Box 4069 Carlton NSW 2218 M 0405 843 933

SFA/NLMC

Drill Method:



Hole ID.

Easting:

BH6

Hole Depth: 14.39 m

4 of 4 Sheet:

Project Name: **Geotechnical Assessment** Project Number: P2160

4-8 Marshall Street, St Leonards NSW Location / Site: Client: **Evergreen Investment Holdings**

Date Completed:

25-FEB-21

Drilling Company: **BG** Drilling Date Started: 26-FEB-21 Ground Level:

Equipment: Track mounted Hanjin Drill Rig Northing:

Method Water Level Depth (m) RL (m)	Graphic Log Material Type	Material Description	Weathering	Estimated Strength (MPa)	D=diametral M or A=axial a 0.69	U.C.S. (Mpa)	ROD %	Core Photo	Defect Spacing (mm)	Defect Description type, inclination, thickness, shape,	Depth (m)	Casing &
Section Sect	Graphic I Bedrock Material	SANDSTONE - grey, fine to coarse grained, trace carbonaceous laminations. Hole Terminated at 14.39 m Target depth achieved	Weatheri Weatheri	XP	A=2.91 D=2.39 A=2.2.2 A=1.97 A=2.08	U.C.S. (A	100 RQD%	Core Pho		roughness coating	14.0 - 15.0 - 16.5 - 17.0 - 17.5	143
Additional Co	omments	5									18.0	



Project No: P2160 Client: Project: Evergreen Investment

4-8 Marshall Street St Leonards

NSW

Contractor: BG Drill Rig: Christie Rig RM/FM



Logged: Approved: AM

Sł	neet	: 1	of 4	14544		Date: 3/02/2022			BH/
Drilling Method	Resistance	Water	Sampling	SSSN	Depth	Stratigraphy	Consistency/ Density	Moisture	Additional Observations
	٦		SPT 7-1 0.5-0.95 m 2,4,5	ML	0.5	TOPSOIL: Sandy SILT, fine to medium grained, dark grey/brown, with rootlets Sandy CLAY, low plasticity, orange-grey fine to medium grained sand (RESIDUAL SOIL)	F	M<	TOPSOIL RESIDUAL SOIL
			2,4,3 N= 9	SC	1.0	Clayey SAND- fine to medium grained, orange/grey/red, low plasticity (RESIDUAL SOIL)	St	PL	
ADT		GWNE	SPT 7-2 1.5-1.95 m 8,12/120mm N= R		1.5	AS ABOVE, with subangular to angular ironstone gravels from 1.4 m (RESIDUAL SOIL) SANDSTONE, fine to medium grained, pale orange, highly weathered, very low strength, with some clay zones (WEATHERED ROCK)			WEATHERED ROCK
	Σ			-	2.5		-	-	
					3.0	Continued as cored hole from 3.0 m			
					3.5				
					4.0				
					5.0				
					5.5				
					6.5				
					7.0				
					7.5 - 8.0				

Project No: P2160 Contractor: MG orrow Client: Drill Rig: Evergreen Investment Christie Rig Project: 4-8 Marshall Street St Leonards Logged: RM/FM Approved: NSW AM Date: Sheet: 2 of 4 3/02/2022 Rock Strength RQD (SCR) Drilling Method Water Depth TCR Stratigraphy Spacing Defect Description ELVL L M H VH 0.03 0.3 0.5 Start Coring at 3.0 m 3.00-3.05, Core loss, 50 mm 3.16, B, 2°, Pl, Ro, Ct clay ΜW SANDSTONE - fine to medium grained, grey-red-orange 3.21, DB 3.40-3.70, core recovered as fragmented rock SANDSTONE - fine to medium grained, grey-red-orange Sandy CLAY- low to moderate plasticity, grey-orange, fine to medium grained sand ММ 3.57, HB RS 3.62, B, 2°, Pl, Ro, Ct carbonaceous material SANDSTONE - fine to medium grained, grey-orange, moderate **%96** 3.67, B, 4°, Un, Ro, Vnr carbonaceous material SW 3.96, B, 4°, Un, Ro, Vnr carbonaceous material 4.00, HB 4.04, HB RS andy CLAY- low to moderate plasticity, grey-orange, fine to medium grained sand 4.20-4.40, core recovered as fragmented rock SANDSTONE - fine to medium grained, grey-orange, moderate 4.53, B, 2°, Pl, Ro, Cn SANDSTONE- fine to medium grained, pale grey-orange, iron SW 4.69, B, 2°, Pl, Ro, Cn bandings with fine to medium angular iron gravels from 4.42-4.47 CORELOSS 4.83-4.93, Core loss, 100mm thk SANDSTONE- Fine to medium grained, pale grey orange, iron 5.16, B, 10°, Pl, Ro, Sn Fe SW 5.24-5.30, CZ, Sn Fe, 60mm thk water loss HW NMLC SW 5.63, B, 2°, Pl, Ro, Ct clay 5.74, B, 5°, Pl, Ro, Cn %0 5.84, B, 1°, Pl, Ro, Cn 5.91, B, 5°, Pl, Ro, Cn 85% 97% 6.00, HB 6.11, HB 6.28, J, 18°, Pl, Ro, Cn MW 6.36, HB 6.5 6.53, HB 6.68, HB SANDSTONE- Pale grey, carbonaceus laminations from 6.9, HB 6.71m 7.06, B, 0°, Pl, Sm, Cn 7.25, V, 10°, Pl, Sm, Cn FR %98 %96 7.90, HB

Project No: Contractor: P2160 MG norrow Client: EverGreen investment Holding Drill Rig: Christie Rig Project: 4-8 Marshall Street St Leonards Logged: FM Approved: NSW AM Sheet: Date: 3/02/2022 Rock Strength Defect Drilling Method RQD (SCR) Water Depth TCR Stratigraphy Spacing Defect Description 0.03 0.3 3 %98 9.16-9.52, B, 5°, Pl, Ro, Cn, 80mm sp %96 SHALE- Fine grained, Dark gray, Flow bandings SANDSTONE- Fine grained, pale grey, massive 10.21, HB 10.36, HB 10.67, HB SANDSTONE- Fine to medium grained, pale 10.82, HB grey,carbonaceous laminations from 10.66 m 10.90, HB NMLC FR 11.81, HB 11.88, HB %86 12.10, HB 12.18, HB 12.38, J, 30°, Pl, Ro, Cn 100% 12.90, HB 13.03, B, 10°, Pl, Ro, Cn 13.07, HB 100% 13.90, HB 13.98, HB Inclusion x1 coarse rounded quartz gravel 14.09, HB End of Borehole at 14.4m Reached Target depth



Project No: Contractor: orrow MG P2160 Client: Drill Rig: Christie Rig Evergreen Investment Project: 4-8 Marshall Street Logged: St Leonards FM **BH8** Approved: NSW AM Sheet: 1 of 3 Date: 7/02/2022 Moisture Resistance Drilling Method USCS Sampling Stratigraphy Additional Observations ${\sf TOPSOIL}\mbox{-} {\sf Sandy}\mbox{ SILT, low plasticity, fine to medium grained}$ TOPSOIL ML sand, dark grey / brown, trace root fibres RESIDUAL SOIL Silty CLAY, medium to high plasticity, yellow/orange, fine to medium subangular to angular ironstone gravel (RESIDUAL SOIL) M< SPT8-1 CI-0.5-0.95 m PL St 3,5,8 N=13 CH SANDSTONE - fine to medium grained, red-purple, highly WEATHERED ROCK ADT weathered, inferred extremely low strength (WEATHERED ROCK) SPT8-2 1.5-1.95 m becoming white / red / orange from 1.6m 5,12,12 N=24 Σ 2.0 Continued as Core Hole from 2.6m

norrow Project No: P2160 Contractor: MG Client: Drill Rig: **Evergreen Investment** Christie Rig Project: 4-8 Marshall Street Logged: St Leonards FM **BH8** NSW Approved: AM Date: Sheet: 2 of 3 7/02/2022 Rock Strength Defect RQD (SCR) Water Depth Spacing TCR Stratigraphy ELVL L M H VHE Start Coring at 2.6 m 2.60-2.71, Core loss, 110mm thk ORE LOSS, 110 mm thick Silty CLAY, medium to high plasticity, grey / red RS 2.81, B, 0°, Pl, Ro, Cn SANDSTONE, fine to medium grained, red 3.0 HW 3.13-3.18, HBx3, 25mm sp 3.42. HB 95% 80% EW 3.51, B, 0°, Pl, Ro, Cn 3.75, B, 0°, Pl, Ro, Cn 3.91-4.00, HBx3, 45mm sp 4.25, B, 0°, Un, Ro, Sn fe 4.28, B, 0°, Pl, Sm, Ct clay 4.32-4.37, DB, Core recovered as fragmented rock becoming red / orange from 4.5 m 4.44, B, 0°, Pl, Ro, Cn 4.75, HB Μ 4.97-5.00, HBx2, 30mm sp W 5.13, HB NMLC 5.35, B, 0°, Pl, Ro, Sn fe 5.47, B, 0°, Pl, Ro, Sn fe SANDSTONE, fine to medium grained, grey, 10° cross beddings 5.53, HB at 2-5mm spacing 100% 5.80, HB 95% 6.0 6.00, HB 6.30, J, 30°, Pl, Ro, Cn 6.5 FR 6.76, J, 30°, Pl, Ro, Cn 6.84, J, 30°, Pl, Ro, Cn SANDSTONE, fine to medium grained, pale grey, massive, some 6.97-7.00, HBx2, 30mm sp carbonaceous laminations 7.10, HB 7.5 SILTSTONE, dark grey, massive 7.50-7.63, DBx7, 20mm sp 100% 100% 7.64, B, 0°, Pl, Ro, Cn 7.95-7.99, Jx2, 35°, Pl, Sl, Cn, 40mm sp

Project No: P2160 Contractor: MG morrow Client: Drill Rig: **Evergreen Investment** Christie Rig Project: 4-8 Marshall Street Logged: St Leonards FM Approved: **BH8** NSW AM Date: Sheet: 3 of 3 7/02/2022 Rock Strength Defect RQD (SCR) Water Spacing TCR Stratigraphy Defect Description ELVL L M HVHE SANDSTONE, fine to medium grained, pale grey, massive 8.05-8.08, Sm, clay, 30mm thk 8.12, HB, 0°, Pl, Ro, Cn 8.55, HB, 0°, Pl, Ro, Cn 85% 70% 9.0 FR 9.00, HB 9.38, HB 9. 9.57, B, 0°, Pl, Ro, Cn 9.59, HB 9.74, HB 9.95-10.00, Core loss, 50mm thk CORE LOSS, 50 mm thick AS ABOVE, SANDSTONE, fine to medium grained, pale grey, massive, some shale inclusions 10. 11.0 10.82, B, 0°, Pl, Ro, Cn 10.93-11.00, HBx2, 70mm sp 11.08-11.30, DBx4, 75mm sp NMLC _ _ _ 11.5 shale clasts, 5-20 mm thick from 11.1 to 11.5m 11.35, J, 45°, Pl, Ro, Cn 11.46, B, 0°, Pl, Sn, Ct clay 11.70, B, 0°, Pl, Ro, Cn 12.18, HB FR 12.52, HB 12.80, HB 13.00, HB 100% 14.00, HB End of Hole at 14.41m



Project No: P2160 Client: Evergreen Investment

Project:

4-8 Marshall Street St Leonards

Drill Rig:

Logged: JA Approved: AM

BG

Christie Rig

Contractor:



BH9 NSW Sheet: 1 of 3 Date: 3/02/2022 Drilling Method USCS Depth Sampling Stratigraphy Additional Observations TOPSOIL / FILL - Silty SAND fine to medium grained, low plasticity with course angular gravel(sandstone), grey SM М SPT9-1 0.5-0.95 m 2,2,1 FILL - sandy clay, low plasticity, grey-brown, trace fine to medium N=3 angular gravel(charcoal), with rootlets Sandy CLAY medium to high plasticity, yellow-brown, fine to medium grained(Residual) M< PL CL- 1.5 ADT SPT9-2 CI yellow mottled orange from 1.6m 1.5-1.95 m 4,5,6 N=11 SANDSTONE fine to medium grained orange-red with clay banding, inferred verry low to low strength, extremely weathered(Weathered Rock) I Continued as cored hole from 3.0m

Project No: P2160 Client: Evergreen Investment Project:

4-8 Marshall Street

NSW

Drill Rig: St Leonards

Logged: JA Approved: AM

BG

Christie Rig

Contractor:



BH9 2 of 3 Date: Sheet: 3/02/2022 Rock Strength Defect RQD (SCR) Drilling Method Water Depth TCR Stratigraphy Spacing Defect Description ELVL L M H VHE 0.03 0.3 0.5 Sandy CLAY I-m plasticity,orange- brown, fine to medium grain sand 3.33-3.56 clay seam RS SANDSTONE fine to medium grained, orange-red, ironstone HW water loss panding 25.00% 100% RS Sandy CLAY m-h plasticity,pale grey , fine to medium grain sand SANDSTONE fine to medium grained, pale grey-orange,patchy MW % Sandy CLAY m-h plasticity,pale grey , fine to medium grain sand SANDSTONE fine to medium grained, orange-red, ironstone 4.0-4.1 core recovered as fragments XW 4.12-BP-5°-PL-RF-Fe Sn anding SANDSTONE fine to medium grained, orange-red, ironstone 4.20-4.56 CLAY SEAM 4.22-BP-2°-PL-RF-Fe Sn 4.32-HB SW SANDSTONE fine to medium grained, grey-orange, 4.66-HB carbonaceous laminations 4.65-HB 4.77-BP-2°-PL-RF-Fe Sn SANDSTONE fine grained, pale grey-red, ironstone banding SW 4.80-BP-2°-PL-RF-Fe Sn 4.82- CLAY SEAM 0% water loss 4.93 - BP-5°-PL-RF-Fe Sn SANDSTONE fine grained, pale grey, inclusion rounded quartz 4.98 - HB %19 SW 5.00 - HB gravel 5.18 - HB SANDSTONE fine grained, pale grey 5.26 - HB SW 5.58 - HB 5.72-5.73 - CLAY SEAM 5.74 - 5.77 - CLAY SEAM SANDSTONE fine to medium grained, grey-orange, ironstone 5.76 -BP-2°-PL-RF-Fe Sn panding and staining 5.98 - HB SANDSTONE fine to medium grained, pale grey-orange, iron 5.99 - HB 6.88 - BP-5°-PL-RF-CN SANDSTONE fine to medium grained, pale grey- red-orange 6.96 - HB 7.42 - BP-1°-PL-RF-CN 7 76 - HB 6.5 7.96 - HB 7.99 - HB SANDSTONE fine to medium grained, pale grey, cross-bedding 5-15°, 5-10mm spacing 0% water loss 100% 100% FR

Project No: P2160 Client: Evergreen Investment Project:

4-8 Marshall Street

Drill Rig: St Leonards

Logged: Approved: BG

Christie Rig

JA

Contractor:



BH9

NSW AM Sheet: 3 of 3 Date: 3/02/2022 Rock Strength Defect Drilling Method RQD (SCR) Water Depth TCR Stratigraphy Spacing Defect Description ELVL L M H VHEI 0.03 0.3 3 as above 8.90 - DB 8.99 - HB as above as above 8.90 - DB 8.99 - HB FR 9.31 - BP-2°-PL-RF- CN 9.7 - HB 9.99 - HB 10.15 - BP-1°-PL-RF-CN 0% water loss FR SHALE dark grey 10.17 - BP-1°-PL-RF-CN SANDSTONE fine to medium grained, pale grey, cross-bedding 5-%66 92% 10.27 - BP-1°-PL-RF-CN 15°, 5-10mm spacing ends at 11.6m 10.38 - BP-1°-PL-RF-CN 10.99 - HB 11.03 - HB 11.19 - BP-1°-PL-RF-CN 11.39 - HB NMIC 11.85 - BP-2°-PL-RF-CN 11.99 - HB FR 0% water loss 100% Carbonaceous Laminations at 13.7m, 10mm spacing 14.48 - BP-2°-PL-RF-Ct x Carbonaceous Laminations 10mm spacing at 14.6m 14.95 - BP-3°-PL-RF-CN 14.99 - HB 15.00 - HB End of Hole at 15.2m Target Depth Reached 15



Project No: Client: Project: P2160 Evergreen Investment

4-8 Marshall Street St Leonards NSW

Contractor: BG Drill Rig: Christie Rig



Logged: Approved: FM/JA RM

	. 1	NSW of 4	'		Approved: RM Date: 4/02/2022			BH10
Drilling Method Resistance	Water	Sampling	USCS	Depth	Stratigraphy	Consistency/ Density	Moisture	Additional Observations
Σ			SM	0.5	TOPSOIL/FILL - Silty SAND fine to medium grained, brown, low plastiticty silt	D	М	
ADT L	GWNE		CI	1.0	Sandy CLAY - medium plasticity, orange-brown, fine to medium grained sand (RESIDUAL)	St	M< PL	
H-M			-	2.0 - 2.5 - 3.0	SANDSTONE - fine to medium grained, white-orange, with clay banding, inferreed very low strength, extremely weathered (WEATHERED ROCK)	-	-	
				3.0 3.5 4.0 4.5 5.5 6.0 7.0 7.5	Continued as cored hole from 3.0 m			

Project No: P2160 Client: Evergreen Investment Project:

4-8 Marshall Street

Drill Rig: St Leonards

BG

Christie Rig

Contractor:



Logged: Approved: Date: FM/JA **BH10** NSW RM Sheet: 7/02/2022 Rock Strength RQD (SCR) Defect Drilling Method Water Depth TCR Stratigraphy Spacing Defect Description 0.03 0.3 3

							1.0			
							3.0	Start Coring 3.0m Sandy CLAY - low to medium plasticity, orange-grey, fine to medium grained sand		
	50% Water Loss	100%	10%		-	RS EW RS	3.5	SANDSTONE fine to medium grained, moderate iron staining Silty CLAY - low to medium plasticity, grey-red		
	\ %0S					HW	4.5	SANDSTONE fine to medium grained, grey, trace fine to medium sub-rounded gravels (ironstone) SANDSTONE fine to medium grained, grey, very thinly bedded		4.00, HB 4.05-4.08, Sm, clay, 30mm thk 4.10, J, 2°, Pl, Ro, Sn Fe 4.39, B, 4°, Pl, Ro, Sn Fe 4.50, HB 4.70, J, 2°, Pl, Ro, Sn Fe
							5.0	LAMINITE fine grained, brown-grey SANDSTONE fine to medium grained with heavy iron staining		4.72-4.74, CZ, 20mm thk 5.00, HB 5.05, B, 2°, PI, Ro, Cn 5.11-5.19, J, 85°, Ir, Ro, Sn Fe
NMLC	50% Water Loss	100%	%98			SW	5.5	SANDSTONE fine to medium grained with carbonaceous laminations at 5° SANDSTONE fine to medium grained, massive with moderate iron staining		5.24, B, 2°, Pl, Ro, Sn Fe 5.25, B, 2°, Pl, Ro, Sn Fe 5.55, HB 5.81, B, 2°, Pl, Ro, Cn 5.87-5.88, Sm, clay, 10mm thk 5.99, B, 2°, Pl, Ro, Cn
	25						6.5	SANDSTONE fine to medium grained with carbonaceous laminations at 5-10°		6.40, HB 6.85, B, 4°, PI, Ro, Cn 6.99, HB
	50% Water Loss	100%	%96			FR	7.5	SANDSTONE fine to medium grained, pale orange, massive		7.60, DB 7.70-7.72, CZ, Ct clay, Sn Fe, 20mm thk 7.75, B, 4°, PI, Ro, Sn Fe 8.00, HB

Project No: P2160 Client: Evergreen Investment Project: 4-8 Marshall Street St Leonards

Contractor: BG Drill Rig: Christie Rig

> Logged: FM/JA RM



BH10 Approved: NSW Sheet: 3 of 4 Date: 7/02/2022 Rock Strength Defect Drilling Method RQD (SCR) Water Depth TCR Stratigraphy Spacing Defect Description ELVL L M H VHE 0.03 0.3 8.00, HB SANDSTONE fine to medium grained, pale grey, massive 8.96, B, 2°, Pl, Ro, Cn 9.0 8.99, HB 9.00, HB 50% Water Loss SANDSTONE fine to medium grained with carbonaceous 9.11, HB laminations at 5-10° 100% %96 9.24, B, 2°, Pl, Ro, Cn 9.42, DB 9.56, B, 2°, Pl, Ro, Cn 9.60, B, 2°, Pl, Ro, Cn 9.63, B, 2°, St, Ro, Cn 9.99, HB 10,0, HB 10.50, HB 10.71, B, 2°, Pl, Ro, Cn 10.77, B, 2°, Pl, Ro, Cn SANDSTONE fine to medium grained, pale grey, massive 11.0 NMLC FR carbonaceous laminations from 11.43-11.8m 50% Water Loss 11.90, HB 12.00, HB 100% 100% 12.09, HB 12.17, HB 12.44, B, 2°, Pl, Ro, Cn 12.55, B, 2°, Pl, Ro, Cn 12. SANDSTONE fine to medium grained with carbonaceous 12.60, DB laminations at 5-10° 13.61, DB 50% Water Loss 14.10, J, 3°, Pl, Ro, Cn 100% End of Borehole at 14.72m Reached Target Depth



POIN	LOAD STRENGTH INDEX	Project No.	P2160
Client:	Evergreen Investment Holdings	Date:	4-Mar-21
Project:	Geotechnical Investigation	Tested by:	MK
Location	4-8 Marshall Avenue, St Leonards NSW	Data checked:	AM

Test Mac	hine:	GSA	Test Local	ity:	MI	HK		Core Size:	52	mm
Bore/TP	Depth (m)	Rock Type	Moisture Condition	Test Type	W (mm)	D (mm)	Load kN (P)	Failure Type	Point Load Strength Index IS ₍₅₀₎ (MPa)	Strength Classification
BH01	2.72	SANDSTONE	F	Α	52.0	41.0	0.81	1	0.30	M
BH01	3.41	SANDSTONE	F	D	50.0	50.0	0.76	2	0.30	М
BH01	3.41	SANDSTONE	F	Α	52.0	41.0	1.24	1	0.47	М
BH01	4.53	SANDSTONE	F	Α	52.0	35.0	0.42	1	0.18	L
BH01	5.07	SANDSTONE	F	D	50.0	49.0	2.99	1	1.23	Н
BH01	5.07	SANDSTONE	F	Α	52.0	46.0	3.60	1	1.24	Н
BH01	6.05	SANDSTONE	F	D	50.0	50.0	1.82	2	0.73	M
BH01	6.05	SANDSTONE	F	Α	52.0	47.0	2.53	1	0.85	M
BH01	7.05	SANDSTONE	F	D	50.0	48.0	3.38	2	1.44	Н
BH01	7.05	SANDSTONE	F	Α	52.0	41.0	5.31	1	1.99	Н
BH01	7.95	SANDSTONE	F	D	50.0	50.0	3.38	1	1.35	Н
BH01	7.95	SANDSTONE	F	Α	52.0	40.0	6.11	1	2.34	Н
BH01	8.57	SANDSTONE	F	D	50.0	50.0	0.52	2	0.21	L
BH01	8.57	SANDSTONE	F	Α	52.0	48.0	0.48	1	0.16	L
BH01	9.05	SANDSTONE	F	D	50.0	50.0	3.06	1	1.22	Н
BH01	9.05	SANDSTONE	F	Α	52.0	39.0	3.20	1	1.25	Н
BH01	10.05	SANDSTONE	F	D	50.0	48.0	4.61	1	1.96	Н
BH01	10.05	SANDSTONE	F	Α	52.0	43.0	4.90	1	1.77	Н
BH01	11.05	SANDSTONE	F	D	50.0	48.0	5.51	1	2.35	Н
BH01	11.05	SANDSTONE	F	Α	52.0	45.0	5.82	1	2.03	Н
BH01	12.29	SANDSTONE	F	D	50.0	48.0	4.39	1	1.87	Н
BH01	12.29	SANDSTONE	F	Α	52.0	45.0	6.40	1	2.23	Н
BH01	13.50	SANDSTONE	F	D	50.0	49.0	4.59	2	1.89	Н
BH01	13.50	SANDSTONE	F	Α	52.0	43.0	6.49	1	2.35	Н
BH01	14.50	SANDSTONE	F	D	50.0	49.0	3.53	2	1.46	Н
BH01	14.50	SANDSTONE	F	Α	52.0	46.0	5.48	1	1.88	Н
TEST TYP) E ·							MOISTURE CON	IDITION :	<u> </u>
								Field (F), Saturat		
	W -		7					i leiu (i), Saturat	ed (3), Dry (D)	
					•		<u> </u>	FAILURE TYPE 1. Fracture throughot influenced by	gh fabric of specin	nen oblique to bedding,
D †	<u> </u>			w Ţ				2. Fracture along	bedding.	
V	V/D > 0.5	D/W = 0.3 - 1.0			V = 0.3 -		3. Fracture influenced by pre-existing joint plane (J), microfracture (M), vein (V), chemical alteration (C).			
DIA	METRAL (D) AXIAL (A)		IR	KEGUL	AR LUMF	· (I)	4. Chip or partial	fracture.	

NOTES For specimens tested parallel to plane of weakness $D_e^2 = D^2$ For specimens tested perpendicular to plane of weakness $D_e^2 = 4WD/\pi$

POIN	I LOAD STRENGTH INDEX	Project No.	P2160
Client:	Evergreen Investment Holdings	Date:	4-Mar-21
Project:	Geotechnical Investigation	Tested by:	MK
Location	: 4-8 Marshall Avenue, St Leonards NSW	Data checked:	AM

Test Mac	hine:	GSA	Test Local	ity:	М	HK		Core Size:	52	mm	
Bore/TP	Depth	Rock Type	Moisture	Test	W	D	Load	Failure Tune	Point Load	Strongth Classification	
	(m)		Condition	Туре	(mm)	(mm)	kN (P)	Failure Type	Strength Index Is ₍₅₀₎ (MPa)	Strength Classification	
BH03	4.31	SANDSTONE	F	D	50.0	51.0	0.09	2	0.03	VL	
BH03	4.31	SANDSTONE	F	Α	52.0	48.0	0.24	1	0.08	VL	
BH03	4.70	SANDSTONE	F	D	50.0	48.0	1.40	2	0.60	M	
BH03	4.70	SANDSTONE	F	Α	52.0	45.0	1.25	1	0.44	M	
BH03	5.40	SANDSTONE	F	D	50.0	50.0	0.43	1	0.17	L	
BH03	5.40	SANDSTONE	F	Α	52.0	44.0	0.57	1	0.20	L	
BH03	6.27	SANDSTONE	F	D	50.0	50.0	0.70	2	0.28	L	
BH03	6.27	SANDSTONE	F	Α	52.0	45.0	2.09	1	0.73	M	
BH03	7.05	SANDSTONE	F	Α	52.0	45.0	0.71	1	0.25	L	
BH03	7.53	SANDSTONE	F	D	50.0	49.0	3.53	1	1.46	Н	
BH03	7.53	SANDSTONE	F	Α	52.0	41.0	4.53	1	1.70	Н	
BH03	8.05	SANDSTONE	F	D	50.0	48.0	4.04	1	1.72	Н	
BH03	8.05	SANDSTONE	F	Α	52.0	45.0	5.43	1	1.90	Н	
BH03	9.05	SANDSTONE	F	D	50.0	49.0	3.70	2	1.53	Н	
BH03	9.05	SANDSTONE	F	Α	52.0	46.0	4.14	1	1.42	Н	
BH03	10.05	SANDSTONE	F	D	50.0	48.0	4.87	1	2.08	Н	
BH03	10.05	SANDSTONE	F	Α	52.0	44.0	5.28	1	1.88	Н	
BH03	11.05	SANDSTONE	F	D	50.0	48.0	3.67	1	1.56	Н	
BH03	11.05	SANDSTONE	F	Α	52.0	41.0	4.41	1	1.65	Н	
BH03	12.05	SANDSTONE	F	D	50.0	48.0	4.43	1	1.89	Н	
BH03	12.05	SANDSTONE	F	Α	52.0	46.0	5.59	1	1.92	Н	
BH03	13.05	SANDSTONE	F	D	50.0	49.0	4.94	1	2.04	Н	
BH03	13.05	SANDSTONE	F	A	52.0	45.0	7.18	1	2.51	Н	
BH03	14.05	SANDSTONE	F	D	50.0	49.0	3.34	1	1.38	Н	
BH03	14.05	SANDSTONE	F	Α	52.0	45.0	4.16	1	1.45	Н	
TEST TYP	E:							MOISTURE CON	IDITION :		
─	W -							Field (F), Saturat	ed (S), Dry (D)		
			₩		•		<mark>⊢ D</mark>	FAILURE TYPE 1. Fracture throughot influenced by	gh fabric of specin	nen oblique to bedding,	
D 1	1	† D		w †				Fracture along	•		
'	V/D > 0.5	D/W = 0.3 - 1.0		DΛ	V = 0.3 -	1.0	3. Fracture influenced by pre-existing joint plane (
-	METRAL (D) AXIAL (A	.)	IR	REGUL	AR LUMF	P (I)	microfracture (M), vein (V), chemical alteration (C). 4. Chip or partial fracture.			

NOTES For specimens tested parallel to plane of weakness $D_e^2 = D^2$ For specimens tested perpendicular to plane of weakness $D_e^2 = 4WD/\pi$

POIN	I LOAD STRENGTH INDEX	Project No.	P2160
Client:	Evergreen Investment Holdings	Date:	4-Mar-21
Project:	Geotechnical Investigation	Tested by:	MK
Location	: 4-8 Marshall Avenue, St Leonards NSW	Data checked:	AM

Test Mac	hine:	GSA	Test Local	ity:	M	HK		Core Size:	52	mm		
Bore/TP	Depth (m)	Rock Type	Moisture Condition	Test Type	W (mm)	D (mm)	Load kN	Failure Type	Point Load Strength Index	Strength Classification		
BH04	4.00	SANDSTONE	F	۸	FO 0	44.0	(P) 2.12	1	IS ₍₅₀₎ (MPa)	M		
BH04	5.12	SANDSTONE	F	A D	52.0	41.0	3.68	1	0.80 1.57	H		
BH04	5.12	SANDSTONE	F	A	50.0 52.0	48.0 46.0	3.31	1	1.57	H		
BH04	6.25	SANDSTONE	F	D	50.0	50.0	2.41	2	0.96	П М		
BH04	6.25	SANDSTONE	F	A	52.0	45.0	4.84	1	1.69	H		
BH04	7.10	SANDSTONE	F	D	50.0	50.0	4.64	2	1.82			
BH04	7.10	SANDSTONE	F	A	52.0	37.0	3.81	1	1.62	<u>Н</u> Н		
BH04	7.10	SHALE/SILTSTONE	F	D	50.0	51.0	0.20	2	0.08	VL		
BH04	7.34	SHALE/SILTSTONE SHALE/SILTSTONE	F	A	52.0	39.0	0.20	1	0.08	L		
BH04	7.40	SHALE/SILTSTONE SHALE/SILTSTONE	F	D		50.0	0.32	2	0.12	L L		
BH04	7.40		F		50.0			3				
		SHALE/SILTSTONE	F	A	52.0	46.0	0.48		0.16	L		
BH04	8.07	SANDSTONE	F	D	50.0	48.0	3.23	2	1.38	H		
BH04	8.07	SANDSTONE	F	A	52.0	46.0	3.80	1	1.30	H		
BH04	9.10	SANDSTONE	•	D	50.0	50.0	2.39	2	0.96	M		
BH04	9.10	SANDSTONE	F	A	52.0	46.0	2.43	1	0.83	M		
BH04	10.17	SANDSTONE	-	D	50.0	50.0	1.64	2	0.66	M		
BH04	10.17	SANDSTONE	F	A	52.0	46.0	2.72	1	0.93	M		
BH04	11.05	SANDSTONE	F	D	50.0	50.0	3.71	2	1.48	H		
BH04	11.05	SANDSTONE	F	Α	52.0	46.0	5.88	1	2.02	H		
BH04	12.39	SANDSTONE	F	D	50.0	48.0	5.06	1	2.16	H		
BH04	12.39	SANDSTONE	F	A	52.0	41.0	5.97	1	2.24	H		
BH04	13.10	SANDSTONE	F	D	50.0	49.0	4.62	1	1.91	Н		
BH04	13.10	SANDSTONE	F	A	52.0	38.0	4.84	1	1.93	H		
BH04	14.20	SANDSTONE	F	D	50.0	48.0	5.48	1	2.34	H		
BH04	14.20	SANDSTONE	F	Α	52.0	44.0	7.23	1	2.57	Н		
TEST TYP	· E ·							MOISTURE CON	IDITION :			
IESI ITP												
	W -		>					Field (F), Saturat	ed (S), Dry (D)			
		1 D		w †	•		D D	FAILURE TYPE: 1. Fracture through fabric of specimen oblique to beddin not influenced by weak planes. 2. Fracture along bedding.				
D/W = 0.3 - 1.0				D/W = 0.3 - 1.0					3. Fracture influenced by pre-existing joint plane (J),			
-	V/D > 0.5 METRAL (AVIAL (A)				AR LUMF	⊃ (I)	microfracture (M), vein (V), chemical alteration (C).				
DIAI	vi⊏ ir∜AL (וט		-			` '	4. Chip or partial fracture.				

NOTES For specimens tested parallel to plane of weakness $D_e^2 = D^2$ For specimens tested perpendicular to plane of weakness $D_e^2 = 4WD/\pi$

POINT LOAD STRENGTH INDEX Project No.		P2160	
Client:	Evergreen Investment Holdings	Date:	4-Mar-21
Project:	Geotechnical Investigation	Tested by:	MK
Location	: 4-8 Marshall Avenue, St Leonards NSW	Data checked:	AM

Test Mac	Test Machine: GSA		Test Local	ity:	MI	-IK		Core Size:	52	mm
Bore/TP	Depth (m)	Rock Type	Moisture Condition	Test Type	W (mm)	D (mm)	Load kN (P)	Failure Type	Point Load Strength Index IS ₍₅₀₎ (MPa)	Strength Classification
BH05	3.37	SANDSTONE	F	D	50.0	50.0	0.54	2	0.22	L
BH05	3.37	SANDSTONE	F	Α	52.0	47.0	1.14	1	0.38	M
BH05	4.38	SANDSTONE	F	D	50.0	50.0	0.88	2	0.35	M
BH05	4.38	SANDSTONE	F	Α	52.0	41.0	0.82	1	0.31	М
BH05	5.18	SANDSTONE	F	D	50.0	51.0	0.16	2	0.06	VL
BH05	5.18	SANDSTONE	F	Α	52.0	42.0	0.89	1	0.33	М
BH05	6.75	SANDSTONE	F	D	50.0	49.0	3.56	2	1.47	Н
BH05	6.75	SANDSTONE	F	Α	52.0	42.0	4.65	1	1.71	Н
BH05	7.10	SANDSTONE	F	Α	52.0	45.0	5.78	1	2.02	Н
BH05	7.05	SANDSTONE	F	D	50.0	50.0	1.14	2	0.46	M
BH05	7.05	SANDSTONE	F	Α	52.0	38.0	5.77	1	2.30	Н
BH05	8.12	SANDSTONE	F	D	50.0	48.0	6.06	1	2.58	Н
BH05	8.12	SANDSTONE	F	Α	52.0	45.0	7.46	1	2.60	Н
BH05	9.05	SANDSTONE	F	D	50.0	49.0	3.15	2	1.30	Н
BH05	9.05	SANDSTONE	F	Α	52.0	40.0	3.77	1	1.44	Н
BH05	10.05	SANDSTONE	F	D	50.0	48.0	4.34	2	1.85	Н
BH05	10.05	SANDSTONE	F	Α	52.0	46.0	5.99	1	2.06	Н
BH05	11.38	SILTSTONE	F	D	50.0	49.0	1.03	2	0.43	M
BH05	11.38	SILTSTONE	F	Α	52.0	41.0	1.07	1	0.40	M
BH05	12.05	SANDSTONE	F	D	50.0	47.0	6.16	1	2.71	Н
BH05	12.05	SANDSTONE	F	Α	52.0	43.0	7.09	1	2.56	Н
BH05	13.05	SANDSTONE	F	D	50.0	48.0	4.46	1	1.90	Н
BH05	13.05	SANDSTONE	F	Α	52.0	41.0	3.77	1	1.41	Н
BH05	14.25	SANDSTONE	F	D	50.0	50.0	3.79	1	1.52	Н
BH05	14.25	SANDSTONE	F	Α	52.0	44.0	4.72	1	1.68	Н
TEST TYP	E:		•					MOISTURE CON	IDITION :	
- 	W -		-			_		Field (F), Saturat	ed (S), Dry (D)	
1 D		W	W W T			D D	FAILURE TYPE: 1. Fracture through fabric of specimen oblique to bedding, not influenced by weak planes. 2. Fracture along bedding.			
D T	V/D > 0.5	D/W = 0.3 - 1.0		D/W = 0.3 - 1.0				Fracture along beauting. Fracture influenced by pre-existing joint plane (J), microfracture (M), vein (V), chemical alteration (C).		
	METRAL (D) AXIAL (A)		IRREGULAR LUMP (I)			4. Chip or partial fracture.			

NOTES For specimens tested parallel to plane of weakness $D_e^{\ 2}$ = D^2 For specimens tested perpendicular to plane of weakness $D_e^{\ 2}$ = $4WD/\pi$

POIN	POINT LOAD STRENGTH INDEX Project No.		P2160
Client:	Evergreen Investment Holdings	Date:	4-Mar-21
Project:	Geotechnical Investigation	Tested by:	MK
Location	4-8 Marshall Avenue, St Leonards NSW	Data checked:	AM

Test Machine: GSA		GSA	Test Local	ity:	MI	HK		Core Size:	52	mm
								•		
Bore/TP	Depth (m)	Rock Type	Moisture Condition	Test Type	W (mm)	D (mm)	Load kN (P)	Failure Type	Point Load Strength Index IS ₍₅₀₎ (MPa)	Strength Classification
BH06	2.70	SANDSTONE	F	D	50.0	48.0	4.68	2	1.99	Н
BH06	2.70	SANDSTONE	F	Α	52.0	45.0	6.20	1	2.16	Н
BH06	3.05	SANDSTONE	F	D	50.0	49.0	3.30	2	1.36	Н
BH06	3.05	SANDSTONE	F	Α	52.0	46.0	3.43	1	1.18	Н
BH06	4.07	SANDSTONE	F	D	50.0	48.0	3.19	2	1.36	Н
BH06	4.07	SANDSTONE	F	Α	52.0	46.0	4.35	1	1.49	Н
BH06	5.07	SANDSTONE	F	D	50.0	50.0	1.49	2	0.60	M
BH06	5.07	SANDSTONE	F	Α	52.0	40.0	1.71	1	0.65	M
BH06	6.05	SANDSTONE	F	D	50.0	50.0	0.92	2	0.37	M
BH06	6.05	SANDSTONE	F	Α	52.0	46.0	1.04	1	0.36	M
BH06	7.07	SANDSTONE	F	D	50.0	49.0	2.92	2	1.21	Н
BH06	7.07	SANDSTONE	F	Α	52.0	42.0	3.69	1	1.36	Н
BH06	8.05	SANDSTONE	F	D	50.0	48.0	4.45	2	1.90	Н
BH06	8.05	SANDSTONE	F	Α	52.0	43.0	4.56	1	1.65	Н
BH06	9.15	SANDSTONE	F	D	50.0	48.0	5.87	1	2.50	Н
BH06	9.15	SANDSTONE	F	Α	52.0	40.0	4.97	1	1.90	Н
BH06	10.05	SANDSTONE	F	D	50.0	48.0	5.02	1	2.14	Н
BH06	10.05	SANDSTONE	F	Α	52.0	39.0	5.84	1	2.28	Н
BH06	11.05	SANDSTONE	F	D	50.0	48.0	4.88	1	2.08	Н
BH06	11.05	SANDSTONE	F	Α	52.0	41.0	5.77	1	2.17	Н
BH06	12.05	SANDSTONE	F	D	50.0	48.0	5.61	1	2.39	Н
BH06	12.05	SANDSTONE	F	Α	52.0	40.0	7.60	1	2.91	Н
BH06	13.05	SANDSTONE	F	D	50.0	48.0	5.16	1	2.20	Н
BH06	13.05	SANDSTONE	F	Α	52.0	43.0	5.54	1	2.00	Н
BH06	14.05	SANDSTONE	F	D	50.0	49.0	5.05	1	2.08	Н
BH06	14.05	SANDSTONE	F	Α	52.0	45.0	5.63	1	1.97	Н
	-							MOIOTURE CC:	ID IT ION	
TEST TYP								MOISTURE CON		
	W -		7					Field (F), Saturat	ea (S), Dry (D)	
		W h			FAILURE TYPE: 1. Fracture through fabric of specimen oblique to bedding, not influenced by weak planes.					
D Ť	WD - 0 =	D/W = 0.3 - 1.0		DΛ	V = 0.3 -	1.0		Fracture along bedding. Fracture influenced by pre-existing joint plane (J),		
	V/D > 0.5 METRAL (AVIAL (A)	IRREGULAR LUMP (I)			P (I)	microfracture (M), vein (V), chemical alteration (C). 4. Chip or partial fracture.			

NOTES For specimens tested parallel to plane of weakness $D_e^{\ 2}$ = D^2 For specimens tested perpendicular to plane of weakness $D_e^{\ 2}$ = $4WD/\pi$

GENERAL

Information obtained from site investigations is recorded on log sheets. The "Cored Drill Hole Log" presents data from an operation where a core barrel has been used to recover material - commonly rock. The "Non-Core Drill Hole - Geological Log" presents data from an operation where coring has not been used and information is based on a combination of regular sampling and insitu testing. The material penetrated in non-core drilling is commonly soil but may include rock. The "Excavation - Geological Log" presents data and drawings from exposures of soil and rock resulting from excavation of pits, trenches, etc.

The heading of the log sheets contains information on Project Identification, Hole or Pit Identification, Location and Elevation. The main section of the logs contains information on methods and conditions, material substance description and structure presented as a series of columns in relation to depth below the ground surface which is plotted on the left side of the log sheet. The common depth scale is 8m per drill log sheet and about 3-5m for excavation logs sheets.

As far as is practicable the data contained on the log sheets is factual. Some interpretation is inevitable in the identification of material boundaries in areas of partial sampling, the location of areas of core loss, description and classification of material, estimation of strength and identification of drilling induced fractures. Material description and classifications are based on SAA Site Investigation Code AS 1726 - 1993 with some modifications as defined below.

These notes contain an explanation of the terms and abbreviations commonly used on the log sheets.

DRILLING

Drilling & Casing

ADV	Auger Drilling with V-Bit
ADT	Auger Drilling with TC Bit
WB	Wash-bore drilling
RR	Rock Roller
NMLC	NMLC core barrel
NQ	NQ core barrel
HMLC	HMLC core barrel
HQ	HQ core barrel

Drilling Fluid/Water

The drilling fluid used is identified and loss of return to the surface estimated as a percentage.

Drilling Penetration/Drill Depth

Core lifts are identified by a line and depth with core loss per run as a percentage. Ease of penetration in non-core drilling is abbreviated as follows:

VE	Very Easy
E	Easy
М	Medium
Н	High
VH	Very High

Groundwater Levels

Date of measurement is shown.

Standing water level measured in completed borehole

Level taken during or immediately after drilling

D	Disturbed
В	Bulk
U	Undisturbed
SPT	Standard Penetration Test
N	Result of SPT (sample taken)
PBT	Plate Bearing Test
PZ	Piezometer Installation
HP	Hand Penetrometer Test

EXCAVATION LOGS

Explanatory notes are provided at the bottom of drill log sheets. Information about the origin, geology and pedology may be entered in the "Structure and other Observations" column. The depth of the base of excavation (for the logged section) at the appropriate depth in the "Material Description" column. Refusal of excavation plant is noted should it occur. A sketch of the exposure may be added.

MATERIAL DESCRIPTION - SOIL

Classification Symbol - In accordance with the Unified Classification System (AS 1726-1993, Appendix A, Table A1)

Material Description - In accordance with AS 1726-1993, Appendix A2.3

Moisture Condition

D	Dry, looks and feels dry
М	Moist, No free water on remoulding
W	Wet, free water on remoulding

Consistency - In accordance with AS 1726-1993, Appendix A2.5

VS	Very Soft	< 12.5 kPa
S	Soft	12.5 – 25 kPa
F	Firm	25 – 50 kPa
St	Stiff	50 – 100 kPa
VSt	Very Stiff	100 – 200 kPa
Н	Hard	> 200 kPa

Strength figures quoted are the approximate range of undrained shear strength for each class.

Density Index. (%) is estimated or is based on SPT results.

VL	Very Loose	< 15 %
L	Loose	15 – 35 %
MD	Medium Dense	35 – 65 %
D	Dense	65 – 85 %
VD	Very Dense	> 85 %

MATERIAL DESCRIPTION - ROCK

Material Description

Identification of rock type, composition and texture based on visual features in accordance with AS 1726-1993, Appendix A3.1-A3.3 and Tables A6a, A6b and A7.

Core Loss

Is shown at the bottom of the run unless otherwise indicated.

Bedding

	_
Thinly Laminated	< 6 mm
Laminated	6 - 20
Very Thinly Bedded	20 - 60
Thinly Bedded	60 - 200
Medium Bedded	200 – 600
Thickly Bedded	600 – 2000
Very Thickly Bedded	> 2000

Weathering - No distinction is made between weathering and alteration. Weathering classification assists in identification but does not imply engineering properties.

Fresh (F)	Rock substance unaffected by weathering
Slightly Weathered	Rock substance partly stained or
(SW)	discoloured. Colour and texture of fresh
	rock recognisable.
Moderately	Staining or discolouration extends
Weathered (MW)	throughout rock substance. Fresh rock
	colour not recognisable.
Highly Weathered	Stained or discoloured throughout. Signs of
(HW)	chemical or physical alteration. Rock texture
	retained.
Extremely	Rock texture evident but material has soil
Weathered (EW)	properties and can be remoulded.

Strength - The following terms are used to described rock strength:

Rock Strength	Abbreviation	Point Load Strength
Class		Index, Is(50)
		(MPa)
Extremely Low	EL	< 0.03
Very Low	VL	0.03 to 0.1
Low	L	0.1 to 0.3
Medium	М	0.3 to 1
High	Н	1 to 3
Very High	VH	3 to 10
Extremely High	EH	≥ 10

Strengths are estimated and where possible supported by Point Load Index Testing of representative samples. Test results are plotted on the graphical estimated strength by using:

Axial Point Load Test

Where the estimated strength log covers more than one range it indicates the rock strength varies between the limits shown.

MATERIALS STRUCTURE/FRACTURES

ROCK

Natural Fracture Spacing - A plot of average fracture spacing excluding defects known or suspected to be due to drilling, core boxing or testing. Closed or cemented joints, drilling breaks and handling breaks are not included in the Natural Fracture Spacing.

Visual Log - A diagrammatic plot of defects showing type, spacing and orientation in relation to core axis.

Defects	 Defects open in-situ or clay sealed	
	 Defects closed in-situ	
	 Breaks through rock substance	

Additional Data - Description of individual defects by type, orientation, in-filling, shape and roughness in accordance with AS 1726-1993, Appendix A Table A10, notes and Figure A2.

Orientation - angle relative to the plane normal to the core axis.

Type BP Bedding Parting JT Joint SM Seam FZ Fracture Zone SZ Shear Zone VN Vein FL Foliation CL Cleavage DL Drill Lift HB Handling Break DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough VYR Very Rough			
SM Seam FZ Fracture Zone SZ Shear Zone VN Vein FL Foliation CL Cleavage DL Drill Lift HB Handling Break DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished S Smooth RF Rough	Туре	BP	Bedding Parting
FZ Shear Zone SZ Shear Zone VN Vein FL Foliation CL Cleavage DL Drill Lift HB Handling Break DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished S Smooth RF Rough		JΤ	Joint
SZ Shear Zone VN Vein FL Foliation CL Cleavage DL Drill Lift HB Handling Break DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished S Smooth RF Rough		SM	Seam
VN Vein FL Foliation CL Cleavage DL Drill Lift HB Handling Break DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished S Smooth RF Rough		FZ	Fracture Zone
FL CL Cleavage DL Drill Lift HB Handling Break DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished S Smooth RF Rough		SZ	Shear Zone
CL Cleavage DL Drill Lift HB Handling Break DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished S Smooth RF Rough		VN	Vein
DL Drill Lift HB Handling Break DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished S Smooth RF Rough		FL	Foliation
HB DB Drilling Break DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished S Smooth RF Rough		CL	Cleavage
DB Drilling Break Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished S Smooth RF Rough		DL	Drill Lift
Infilling CN Clean X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		НВ	Handling Break
X Carbonaceous Clay Clay KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		DB	Drilling Break
Clay KT CA CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough	Infilling	CN	Clean
KT Chlorite CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		x	Carbonaceous
CA Calcite Fe Iron Oxide Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		Clay	Clay
Fe		КТ	Chlorite
Qz Quartz MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		CA	Calcite
MS Secondary Mineral MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		Fe	Iron Oxide
MU Unidentified Mineral Shape PR Planar CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		Qz	Quartz
Shape PR CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		MS	Secondary Mineral
CU Curved UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		MU	Unidentified Mineral
UN Undulose ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough	Shape	PR	Planar
ST Stepped IR Irregular DIS Discontinuous Rougness POL Polished SL Slickensided S Smooth RF Rough		CU	Curved
Rougness POL Polished SL Slickensided S Smooth RF Rough		UN	Undulose
Rougness POL Polished SL Slickensided S Smooth RF Rough		ST	Stepped
Rougness POL Polished SL Slickensided S Smooth RF Rough		IR	Irregular
SL Slickensided S Smooth RF Rough		DIS	Discontinuous
S Smooth Rough	Rougness	POL	Polished
RF Rough		SL	Slickensided
		S	Smooth
VR Very Rough		RF	Rough
		VR	Very Rough

SOIL

Structures - Fissuring and other defects are described in accordance with AS 1726-1993, Appendix A2.6, using the terminology for rock defects.

Origin - Where practicable an assessment is provided of the probable origin of the soil, eg fill, topsoil, alluvium, colluvium, residual soil.

[°] Diametral Point Load Test

IMPORTANT INFORMATION



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